Systematic simulation studies on the penetration of resonant magnetic perturbations in EAST

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7 Abstract: The penetration properties of the n = 1 resonant magnetic perturbations (RMPs) with 8 toroidal rotation are systematically studied by the upgraded three-dimensional toroidal 9 magnetohydrodynamic code CLTx. Through both linear and nonlinear simulations, it is found that 10 in the presence of toroidal plasma rotation, the saturation state for high resonant harmonics is 11 obtained in linear simulations due to the mode becoming unlocked from the internal magnetic 12 islands. While in nonlinear simulations, nonlinear effects become important when the toroidal 13 plasma rotation is not included. The zonal component resulted from the nonlinear mode coupling is necessary for the saturation of the whole system including the internal kink mode and the m/n = 2/114 tearing mode. The simulations on RMP penetration demonstrate that the mode coupling is associated 15 16 with the toroidal effect rather than a consequence of nonlinear effects. With a low resistivity, the 17 single-harmonic-RMP is hard to penetrate the mode-rational surface because of the plasma 18 screening effect, resulting in a truncation on the radial mode structure. On the other hand, the non-19 resonant components in the multiple-harmonic-RMP could largely reduce the effect of the plasma 20 shielding and result in that the RMP is able to penetrate deeply into the central plasma region through 21 the poloidal harmonics coupling.

22 Keywords: resonant magnetic perturbation, penetration, nonlinear effects, toroidal effect

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31 1 Introduction

Resonant magnetic perturbation (RMP) is very efficient for controlling the edge localized mode (ELM) [1] in H-mode [2] discharge in Tokamaks. However, MHD (magnetohydrodynamic) theoretical analysis [3, 4], numerical simulations [5-18], and plasma experiments [19-21] have demonstrated that RMP penetration theory based on the vacuum model is inaccurate or even completely invalid. Meanwhile, RMP penetration is especially sensitive to plasma response in the presence of dynamical effects, like plasma rotation [11, 22], two-fluid effects [9, 12, 23, 24], screen current [25, 26], nonlinear mode coupling [6, 9, 17, 27], etc.

39 Linearized models in analytical and numerical studies of the influence of plasma response on 40 RMP penetration have been widely adopted and have shown high efficiency in calculation speed and great feasibility compared with plasma experimental results. Results obtained by the MARS-F 41 42 code based on a linearized single-fluid MHD model have successfully explained the offset of the optimal coil phase in edge localized mode (ELM) control experiments with the n = 1 and 2 RMPs 43 in EAST (Experimental Advanced Superconducting Tokamak) [10, 28] and the n = 2 RMP in the 44 ASDEX Upgrade (Axially Symmetric Divertor Experiment) [28, 29], where n represents the 45 46 toroidal mode number. The simulation results from the M3D-C¹ code adopting a linearized two-47 fluid model have demonstrated that the penetrated RMP field reaches its maximum value when the 48 perpendicular electron rotation vanishes at the mode-rational surface [12, 24]. However, nonlinear 49 simulations of RMPs have indicated that nonlinear effects are crucial and exhibit some dynamical 50 features that are not present in purely linear simulations, such as the density pumpout due to the n= 0 component coupled with n = 2 perturbations [6] and the generation of high-order magnetic 51 52 islands from the coupling of different harmonics [9]. In addition, the resonant amplification of RMPs 53 due to the coupling between the non-resonant kink component (|m| > |nq|), where m is the poloidal 54 mode number, and q is the safety factor) and the resonant m component has been observed in both 55 linear and nonlinear modelings, respectively, by the MARS-F code [30] and the JOREK code [6], 56 The validity criterion for the linear model can be written simply as the overlap condition $\left|\partial \zeta_r / \partial r\right| < 1$ (where ζ_r is the plasma displacement normal to the equilibrium magnetic field) 57 after considering plasma response [27, 28]. Although the linear model has the advantages of being 58 59 numerically and analytically efficient while still maintaining great validity in RMP calculations, 60 nonlinear mode couplings, however, should not be ignored in some cases [27, 28].

61 In our previous work [18], the code CLT was upgraded to CLTx for studying RMP penetration

62 in EAST based on the linear and nonlinear resistive MHD equations. Results from linear simulations 63 of RMPs applied to studies regarding ELM mitigation discharge 52340 in EAST have agreed well 64 with those obtained from the MARS-F code. However, subsequent numerical simulation studies with different adopted resistivities suggest that the amplitude reduction and the phase shift of the 65 66 resonant harmonics due to plasma response increase with decreasing resistivity. In this work, the 67 nonlinear terms are retained in the CLTx code for studying the nonlinear effects on RMP penetration. 68 The influences of toroidal rotation, nonlinear mode coupling, and toroidal effect on RMP penetration 69 will be analyzed and discussed. The outline of the present paper is as follows: Section 2 introduces 70 the simulation model used in the CLTx code; Section 3 presents the results of the linear and 71 nonlinear simulations for RMP penetration and the influences of toroidal rotation; Section 4 gives 72 the toroidal effect on RMP penetration in detail; and finally, the results of the present paper are 73 summarized in Section 5.

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- 75 2 Simulation model for CLTx

In the CLTx code, we adopted the full set of single fluid, resistive MHD equations including
dissipations [18, 31], i.e.,

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$$\partial_t \rho = -\nabla \cdot (\rho \mathbf{v}) + \nabla \cdot [D\nabla (\rho - \rho_0)], \qquad (1)$$

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$$\partial_t p = -\mathbf{v} \cdot \nabla p - \Gamma p \nabla \cdot \mathbf{v} + \nabla \cdot \left[\kappa \nabla \left(p - p_0 \right) \right], \qquad (2)$$

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$$\partial_t \mathbf{v} = -\mathbf{v} \cdot \nabla \mathbf{v} + \left(\mathbf{J} \times \mathbf{B} - \nabla p\right) / \rho + \nabla \cdot \left[\nu \nabla \left(\mathbf{v} - \mathbf{v}_0\right)\right], \tag{3}$$

 $\partial_t \mathbf{B} = -\nabla \times \mathbf{E} \,, \tag{4}$

82 with

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$$\mathbf{E} = -\mathbf{v} \times \mathbf{B} + \eta \left(\mathbf{J} - \mathbf{J}_{\mathbf{0}} \right), \tag{5}$$

$$\mathbf{J} = \nabla \times \mathbf{B}, \tag{6}$$

85 where ρ , p, \mathbf{v} , \mathbf{B} , \mathbf{E} , and \mathbf{J} are the plasma density, thermal pressure, plasma velocity, 86 magnetic field, electric field, and current density, respectively. The subscript '0' denotes equilibrium quantities. Γ (= 5/3) is the ratio of specific heat of the plasma. The variables are normalized as: 87 $\mathbf{B} / B_{00} \rightarrow \mathbf{B} \ , \quad \mathbf{x} / a \rightarrow \mathbf{x} \ , \quad \rho / \rho_{00} \rightarrow \rho \ , \quad \mathbf{v} / v_A \rightarrow \mathbf{v} \ , \quad t / \tau_A \rightarrow t \ , \quad p / \left(B_{00}^2 / \mu_0 \right) \rightarrow p \ ,$ 88 $\mathbf{J}/(B_{00}/\mu_0 a) \rightarrow \mathbf{J}$, $\mathbf{E}/(v_A B_{00}) \rightarrow \mathbf{E}$, and $\eta/(\mu_0 a^2/\tau_A) \rightarrow \eta$, where *a* is equal to one meter, 89 $v_A = B_{00} / \sqrt{\mu_0 \rho_{00}}$ is the Alfvén speed, and $\tau_A = a / v_A$ is the Alfvén time. B_{00} and ρ_{00} are the 90 91 initial magnetic field and plasma density at the magnetic axis, respectively. Note that the Hall term [32] in the generalized Ohm's law is not included, thus diamagnetic drifts due to two-fluid effects 92

are not present in the current model.

94 The simulation domain constructed in the CLTx code has been extended beyond the last closed 95 magnetic surface to the scrape-off layer (SOL) with the inclusion of the X-point. The normalized parameters used in all simulations herein are fixed to be $D = 1 \times 10^{-6}$, $\kappa = 5 \times 10^{-5}$, and 96 $\mu = 1 \times 10^{-6}$. The spatial distribution of the time-independent resistivity is determined by the initial 97 normalized plasma temperature T with $\eta = \eta_0 \cdot T^{-3/2}$, where η_0 is the resistivity at the 98 99 magnetic axis and corresponds to a resistivity minimum since the temperature is maximum at this 100 axis. A mesh consisting of $256 \times 16 \times 256$ points in (R, ϕ, Z) is utilized for all simulations. In the CLTx code, the basic straight field line coordinates $(\sqrt{\psi_n}, \theta_s, \phi)$ [18, 33] are used for spectrum 101 analysis, where $\sqrt{\psi_n}$ is the square root of the normalized poloidal flux ψ_n , θ_s is the 102 103 generalized poloidal angle, and ϕ is the toroidal angle.

The initial equilibria are reconstructed from EAST discharge 52340 at 3150 ms [10] and discharge 62585 at 3800 ms [34] by EFIT (Equilibrium Fitting code) [35]. The safety factor qprofiles for each discharge and the toroidal rotation ω_t profile of discharge 52340 are given in Figure 1.



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Figure 1. Initial profiles of the safety factor q for EAST discharge 52340 at 3150 ms and 62585 at 3800 ms, and the toroidal rotation ω_t for EAST discharge 52340 at 3150 ms.

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112 **3** Linear and nonlinear saturations with the presence of RMP

In our previous linear benchmark study for the equilibrium of discharge 52340, the magnetic island at high rational surfaces (q > 1) reaches a level of significant saturation, however the inner unstable m/n = 1/1 kink mode is still in the linear growth stage [18]. To understand the detailed saturation mechanisms of magnetic islands in linear simulations, comparisons between linear and nonlinear simulations with a relatively large resistivity $\eta_0 = 5 \times 10^{-7}$ are performed in the present paper. The RMP coils set up in the CLTx code is $I_{coil} = 10$ kAt (kilo-Amp-turns), n = 1, $\Delta \Phi = 0$, 119 where $\Delta \Phi$ is the relative phase difference between the upper and lower coils [28]. The role of the 120 plasma toroidal rotation on mode saturation is also studied in the present paper by artificially 121 including plasma rotation, however, the artificial toroidal rotation speed is constrained to be sub-122 sonic. Under these conditions, the resultant inertial force on the equilibria due to toroidal rotation is 123 less than one percent of the entire pressure gradient force and is not included in the governing 124 equations of the CLTx code initially. The same considerations are taken for discharges 52340 and 125 62558 discussed below.





127 Figure 2. Time evolutions of resonant harmonics $b_{m/n}^r$ at different rational surfaces with both 128 linear (dashed lines with circles, indicated by 'L', the same below) and nonlinear (solid lines, indicated by 'NL', the same below) simulations for discharge 52340 (a) with toroidal rotation (the 129 m/n = 1/1 harmonics are artificially reduced by multiplying a factor of 0.02) and (b) without toroidal 130 131 rotation, as well as for discharge 62585 (c) with toroidal rotation (the m/n = 2/1 harmonics are 132 artificially reduced by multiplying a factor of 0.25) and (d) without toroidal rotation. The vertical 133 axes of the left-hand side panels are scaled linearly, while the vertical axes of the right-hand side 134 panels are scaled logarithmically.

Time evolutions of resonant harmonics $b_{m,n}^r$ driven by RMP for the equilibrium of discharge 136 52340 with the toroidal rotation are shown in Figure 2 (a). Nonlinear effects in the pedestal region 137 $(m \ge 5, n = 1)$ are ignorable but the chosen resistivity $\eta_0 = 5 \times 10^{-7}$ is artificially enlarged by two 138 orders of magnitude compared with the experimental parameter. Evidently, the only significant 139 140 difference between the linear and nonlinear simulations is that the unstable m/n = 1/1 kink mode becomes saturated due to nonlinear mode coupling after 2100 τ_A . These results suggest that 141 142 nonlinear effects are not important before the internal kink instability begins to play a role in the overall plasma dynamics, although it should be noted that the islands overlap condition 143 144 $\left|\partial \zeta_r / \partial r\right| < 1$ [27, 28] is not satisfied in the pedestal after taking the plasma response into account 145 [18].

Figure 2 (b) shows the simulation results for discharge 52340 without the toroidal rotation. No saturation for any harmonic is observed in the linear result without toroidal rotation. While in the nonlinear case, the m/n = 1/1 kink mode becomes saturated as expected due to nonlinear mode coupling, which also contributes to the reduction of higher harmonics ($m \ge 2, n = 1$).

The second set of simulations with EFIT reconstructed equilibrium for EAST discharge 62585 150 151 at 3800 ms [34] is carried out both with and without the toroidal rotation. All parameters and the 152 RMP configurations are the same as those in the preceding simulations. The safety factor profile of 153 discharge 62585 is monotonous with $q_{min} = 1.59$ and $q_{95} = 4.87$ as shown in Figure 1. The toroidal rotation profile of discharge 52340 in Figure 1 is artificially added in the static equilibrium 154 155 of discharge 62585 due to the lack of a self-consistent rotation profile. The results of discharge 156 62585 in Figure 2 (c) and (d) show similar tendencies in comparison with those of discharge 52340. All resonant harmonics with high poloidal mode number ($m \ge 3$, n = 1) become saturated both with 157 158 and without toroidal rotation in both the linear and nonlinear simulations. Uniquely, the lowest 159 resonant m/n = 2/1 tearing mode exhibits a continuous growth (the oscillation of the m/n = 2/1160 tearing mode is due to the mode rotating with the toroidal flow) in its linear simulation, while in the 161 nonlinear simulation this particular mode becomes saturated due to the generation of the n = 0 zonal component through nonlinear mode coupling [36, 37]. 162

Similar saturated time-independent solutions for stable equilibria were reported in the linearized MHD simulations carried out with the M3D-C¹ code [24]. However, in our simulations of unstable equilibria with the toroidal rotation, the linearly saturated solutions for the n = 1 RMP are obtained for the harmonics with $m \ge 2$ in discharge 52340 and $m \ge 3$ in discharge 62585 with

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the presence of toroidal rotation. The same saturated results for high harmonics obtained in both
linear and nonlinear simulations with the toroidal rotation further demonstrate the validity of the
linear model used in the previous researches of the MARS-F and CLTx code [10, 18].

With different amplitudes of RMP Icoil = 5kAt, 10kAt, and 20kAt, the time evolutions of the 170 171 m/n = 4/1 harmonic at the q = 4 rational surface for EAST discharge 52340 with the toroidal rotation 172 are given in Figure 3. The shielding effects due to plasma response are almost identical for all cases 173 with the shielding ratio $(b_{response}^r / b_{vacuum}^r)$ approaching approximately 60%. Meanwhile, the overall 174 qualitative evolutions among all cases are almost identical, that is, the modes for all cases become 175 saturated after 3000 τ_A . The saturation amplitude of the high resonant harmonic with plasma 176 response is linearly proportional to the intensity of the vacuum RMP. Also, the increase of the RMP 177 intensity does not lead to breakdown of high resonant harmonics.



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Figure 3. Time evolutions of resonant harmonics $b_{m/n}^r$ at the q = 4 rational surface for EAST discharge 52340 with toroidal rotation. The amplitude of the RMP is adjusted by 5 kAt (blue), 10 kAt (red), and 20 kAt (green). The hexagrams along the vertical axis mark out the amplitudes of the resonant m/n = 4/1 harmonic in vacuum for each case.

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184 4 Toroidal effect on the penetration of RMP

In this section, we mainly focus on toroidal coupling effect on penetration of RMP in the interior resonant surfaces. Thus, the SOL region is not included in this study. In order to reduce the impact of boundary treatment, the safety factor for discharge 52340 is truncated to a finite value at the plasma boundary and the q = 6 rational surface is slightly shifted inward. The reconstructed equilibrium from the QSOLVER code [38] is shown by the red line of Figure 7. The RMP field is applied inside the plasma boundary where the generalized poloidal angle θ_s can be defined accurately. Usually, RMP fields generated by realistic coils contain multiple resonant and nonresonant harmonics and the penetration of a specific harmonic could be influenced by others [6, 30]. In this section, instead of the RMP fields directly calculated from the realistic coils, we chose the RMP to be artificially composited with different harmonics of the perturbed magnetic flux $\delta \psi_{\rm RMP}$ as follows,

$$\delta \psi_{\mathbf{RMP}} = \sum_{m,n} \delta \psi_{m,n} \cos\left(m\theta_s(\psi_n) + n\phi\right) \left(1 + \tanh\left(\left(\psi_n - \psi_0\right)/d_{RMP}\right)\right) / m, \qquad (7)$$

197 where $\delta \psi_{m,n}$ is on the order of 10⁻⁵, corresponding to currents of several kiloamperes (kA), ψ_n 198 is the normalized poloidal flux, $\psi_0 = 0.90$, and $d_{RMP} = 0.02$.

With varying combinations of different RMP harmonics, the response of the radial perturbation 199 of the resonant magnetic field $b_{m/n=2/1}^r$ at the q = 2 rational surface is investigated. The reason for 200 201 choosing the q = 2 surface is that the penetration mechanisms for different harmonics should be 202 qualitatively consistent and the spectrum analysis is more accurate for lower harmonics. In the first 203 subsection below, we discuss the simulation results of the single-harmonic-RMP and the double-204 harmonic-RMP, in which the different roles played by resonant and non-resonant components will 205 be illustrated. In the second subsection, the poloidal harmonics filtering analysis and the multiple-206 harmonic-RMP simulation results are presented to confirm the importance of poloidal harmonics 207 coupling on RMP penetration.

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209 4.1 The single-harmonic-RMP and the double-harmonic-RMP

210 In this subsection, the single-harmonic-RMP is chosen to be two different amplitudes with $\delta \psi_{2,1} = 2 \times 10^{-5}$ and $\delta \psi_{2,1}(\times 2) = 4 \times 10^{-5}$ while the double-harmonic-RMP consists of the $m/n = 10^{-5}$ 211 2/1 harmonic and another higher m harmonic (m > 2, n = 1) with the same amplitude 212 $\delta \psi_{m,n} = 2 \times 10^{-5}$. A large resistivity ($\eta_0 = 10^{-6}$) is used and all simulations are carried out based on 213 the fully nonlinear simulation code CLT. Figure 4 shows time evolutions for $b_{m/n=2/1}^r$ with two 214 different harmonic compositions of RMP. It is evident that, compared with the single m/n = 2/1215 harmonic RMP with $\delta \psi_{2,1} = 2 \times 10^{-5}$, an extra higher harmonic (m > 2) of RMP results in a larger 216 tearing mode response at the q = 2 rational surface. In particular, the amplitude of $b_{m/n=2/1}^{r}$ under 217 the m/n = 2/1+4/1 RMP is the largest among all cases with higher harmonic superposition (m > 2), 218 but still remains less than that of the m/n = 2/1 (×2) RMP with $\delta \psi_{2,1}(\times 2) = 4 \times 10^{-5}$. Consequently, 219 the higher harmonics (m > 2) of the RMP could generate considerable driving effects at the q = 2220 221 rational surface.



Figure 4. Time evolutions of $b_{m/n=2/1}^r$ with different harmonic compositions of RMP. The double-







Figure 5. Time evolutions for amplitudes of $b_{m/n=2/1}^r$ with different harmonic compositions of RMP. The results from single-harmonic-RMP ($\delta \psi_{2,1} = 4 \times 10^{-5}$) are plotted using blue lines, while red lines represent results from the double-harmonic-RMP ($\delta \psi_{2,1} = 2 \times 10^{-5}$, $\delta \psi_{6,1} = 6 \times 10^{-5}$). The resistivities used in each simulation are (a) $\eta_0 = 10^{-8}$, (b) $\eta_0 = 10^{-7}$, (c) $\eta_0 = 10^{-6}$, and (d) $\eta_0 = 10^{-5}$, respectively.

233 In order to further understand how the higher harmonic to enhance the tearing mode response at the q = 2 rational surface, another comparison study is carried out by using different values of the 234 resistivity based on two sets of RMP configuration with (a) $\delta \psi_{21} = 4 \times 10^{-5}$ (the single-harmonic-235 RMP), (b) $\delta \psi_{2,1} = 2 \times 10^{-5}$ and $\delta \psi_{6,1} = 6 \times 10^{-5}$ (the double-harmonic-RMP), respectively. A 236 relatively large m = 6 component is applied to the double-harmonic-RMP to strengthen its driving 237 effect. The time evolutions of $b_{m/n=2/1}^r$ at the q=2 surface with different RMP configurations are 238 plotted in Figure 5. When the resistivity is small, such as $\eta_0 = 10^{-8}$ shown in Figure 5 (a), the 239 240 driving effect of the m = 6 harmonic at the q = 2 rational surface is relatively weak, resulting in the 241 amplitude of $b_{m/n=2/1}^r$ becoming smaller in the double-harmonic-RMP compared to that in the single-harmonic-RMP. However, when the resistivity increases, the driving effect from the higher 242 harmonic becomes more important. After the resistivity increases to $\eta_0 = 10^{-6}$ shown in Figure 5 243 (c), the amplitude of $b_{m/n=2/1}^r$ in the double-harmonic-RMP exceeds that of the single-harmonic-244 RMP. 245

Figure 6 exhibits the $b_{n=1}^{r}$ spectra corresponding to the cases in Figure 5 (a) and (c). For the 246 low resistivity $\eta_0 = 10^{-8}$, as shown in Figure 6 (a) and (b), the penetration depth of m = 2 harmonic 247 248 is limited outside the q = 2 rational surface for both types of RMPs. The m = 6 harmonic vanishes 249 quickly before reaching the q = 2 surface. Consequently, the resultant m = 2 and m = 6 perturbations from the double-harmonic-RMP are almost independent of each other, and the $b_{m/n=2/1}^r$ is mainly 250 driven by the m = 2 harmonic of the RMP. The spectrum is consistent with that shown in Figure 5 251 (a), where the amplitude of $b_{m/n=2/1}^r$ from the double-harmonic-RMP is lower than that of the 252 single-harmonic-RMP. However, after the resistivity increases to $\eta_0 = 10^{-6}$, the penetration depths 253 254 from both types of RMP are greatly boosted, which suggests that the large resistivity can largely reduce the current shielding and enhance the penetration of RMPs. Meanwhile, the results from the 255 256 double-harmonic-RMP also become completely different. Due to the toroidal effect, the strong m =6 harmonic in RMP generates a sequence of lower $b_{m,n}^r$ harmonics from m = 5 to m = 2 and 257 258 propagates inward to the central plasma region. The longest arrow in Figure 6 (d) indicates the 259 inward propagation direction of the RMP from the m = 6 harmonic to the m = 2 harmonic due to the toroidal effect. After successful penetration by the higher harmonic, the considerable m = 3 and m260 = 4 components are generated at the q = 2 rational surface, which could indirectly drive $b_{m/n=2/1}^r$. 261 In addition, the $b_{m/n=2/1}^r$ component inside the q = 2 rational surface is also much larger than that 262 263 of the single-harmonic-RMP. Therefore, for the double-harmonic-RMP, the inside and outside resonant driving (m = 2) and the non-resonant driving (m > 2) together result in the final amplitude of $b_{m/n=2/1}^r$ to exceed that of the single-harmonic-RMP, even though the direct m = 2 driving strength from the double-harmonic-RMP is only a half of the single-harmonic-RMP.



Figure 6. The radial distributions of the $b_{n=1}^r$ spectra at $t = 423\tau_A$ for (a) the single-harmonic-RMP ($\delta \psi_{2,1} = 4 \times 10^{-5}$, $\eta_0 = 10^{-8}$), (b) the double-harmonic-RMP ($\delta \psi_{2,1} = 2 \times 10^{-5}$, $\delta \psi_{6,1} = 6 \times 10^{-5}$, $\eta_0 = 10^{-8}$), (c) the single-harmonic-RMP ($\delta \psi_{2,1} = 4 \times 10^{-5}$, $\eta_0 = 10^{-6}$), and (d) the double-harmonic-RMP ($\delta \psi_{2,1} = 2 \times 10^{-5}$, $\delta \psi_{6,1} = 6 \times 10^{-5}$, $\eta_0 = 10^{-6}$).

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273 The influences from the intrinsic kink and tearing instabilities (m/n = 1/1 resistive kink mode 274 and m/n = 2/1 tearing mode) on the RMP penetration process is further examined by using artificially setting-up resistivity distribution. Two types of artificial resistivity distributions are shown in Figure 275 7. With the type-1 distribution, the small resistivity value ($\eta_0 = 10^{-8}$) is applied inside the q = 1276 277 rational surface to reduce the growth rate of the m/n = 1/1 resistive kink mode, while the resistivity in the outer region (q > 1) remains at a high level ($\eta_0 = 10^{-6}$). It is found that, in comparison with 278 279 the results of Figure 5 (c), the lower resistivity inside the q = 1 surface has a little effect on the evolution of $b_{m/n=2/1}^r$ at the q=2 surface. As shown in Figure 8, the only difference resulted from 280 281 the type-1 resistivity distribution is that $b_{m/n=1/1}^r$ at the q = 1 rational surface becomes much weaker

because magnetic reconnection is suppressed due to the small resistivity. While the global mode structures of $b_{m/n}^r$ outside the q = 1 rational surface are almost identical between these two cases. Consequently, the fast growth of the m/n = 1/1 harmonic is the result of the external driving process rather than the intrinsic resistive kink instability.





Figure 7. Profile of the safety factor (red line) reconstructed for discharge 52340 with the QSOLVER code and the two different types of the resistivity η_0 distributions: Type-1 (black line), the small resistivity value ($\eta_0 = 10^{-8}$) is applied inside the q = 1 rational surface, but the resistivity in the outer region (q > 1) remains at a high level ($\eta_0 = 10^{-6}$); Type-2 (blue line), the small resistivity value ($\eta_0 = 10^{-8}$) is applied inside the q = 2 rational surface, but the resistivity in the outer region (q > 2) keeps at a high level ($\eta_0 = 10^{-6}$).





Figure 8. The radial structures of $b_{m,n}^r$ at $t = 800\tau_A$ with the double-harmonic-RMP for (a) the uniform η_0 resistivity distribution, $\eta_0 = 10^{-6}$, (b) the type-1 resistivity distribution with $\eta_0^{q \le 1} = 10^{-8}$ and $\eta_0^{q > 1} = 10^{-6}$.

298 With the type-2 resistivity distribution (the lower resistivity inside the q = 2 rational surface), 299 the penetration properties of the single-harmonic-RMP and the double-harmonic-RMP become 300 totally different. Firstly, due to the generation of the screen current, a strong shielding effect is 301 observed in the mode structures of $b_{m/n=2/1}^r$ in Figure 9 (a) and δE_{ϕ} in Figure 10 (a). Thus, the 302 single-harmonic-RMP penetration is blocked at the q = 2 rational surface, and the amplitude of the $b_{m/n=2/1}^{r}$ component inside the q=2 surface is much weaker than that outside the surface. In contrast, 303 304 with the double-harmonic-RMP applied as shown in Figure 9 (b), a series of intermediate non-305 resonant harmonics (*m* from $3\sim 5$) are greatly generated across the entire space. As a result, with the 306 double-harmonic-RMP, the penetrated $b_{m/n=2/1}^r$ component inside the q = 2 surface is comparable 307 with that outside the surface. With the indirect driving from non-resonant harmonics $(m \ge 2)$ at the 308 rational surface and the direct driving from resonant harmonic (m = 2) both inside and outside, the 309 value of $b_{m/n=2/1}^r$ at the q=2 surface far exceeds that of the single-harmonic-RMP, even though the external m = 2 driving strength in the single-harmonic-RMP case is doubled. Meanwhile, as 310 shown in Figure 10 (b), the m/n = 1/1 perturbation resulted from the double-harmonic-RMP 311 312 penetrates deeply into the central core region, and consequently, a strong kink mode is excited inside 313 the q = 1 rational surface.



Figure 9. The radial structures of $b_{m,n}^r$ at $t = 800\tau_A$ with the type-2 resistivity distribution $(\eta_0^{q\leq 2} = 10^{-8} \text{ and } \eta_0^{q>2} = 10^{-6})$ for (a) the single-harmonic-RMP, (b) the double-harmonic-RMP.



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Figure 10. The mode structures of δE_{ϕ} at $t = 800\tau_A$ with the type-2 resistivity distribution, $\eta_0^{q \le 2} = 10^{-8}$ and $\eta_0^{q > 2} = 10^{-6}$ for (a) the single-harmonic-RMP, and (b) the double-harmonic-RMP. 320

321 4.2 Poloidal harmonic filtering analysis and the multiple-harmonic-RMP

322 A supplementary study concerning the toroidal effect on RMP penetration was carried out using 323 poloidal filtering analysis. The filtering analysis is applied in the linear EAST RMP simulation where the SOL has been retained and the vacuum RMP field is calculated based on the realistic 324 325 RMP coils [18]. Because the Cartesian grids in the poloidal section are used in the CLTx code, 326 poloidal filtering analysis demands two coordinate transformations with interpolations among 327 Cartesian grids and magnetic flux grids inside the plasma boundary for carrying out the Fourier 328 transformations while an asymptotic transition is applied between the plasma and SOL regions for 329 numerical continuity. The original radial structure of $b_{m,n}^r$ under the n = 1 EAST RMP is plotted in 330 Figure 11 (a). To analyze the numerical errors resulting from the interpolations from coordinate 331 transformations, we conducted a controlling simulation by employing the interpolations and Fourier 332 transformations while all harmonics are retained in the inverse Fourier transformation. The results 333 shown in Figure 11 (b) indicate that the numerical errors due to these processes only lead to a limited 334 decline of the m = 2 harmonic, but the errors' influences on higher harmonics ($m \ge 3$) are ignorable. After we removed the m = 4 component in the inverse Fourier transformation, the global amplitude 335 of m = 3 is greatly reduced and its maximum value is almost only a half of its original level as shown 336 in Figure 11 (c). Next, as shown in Figure 11 (d), after we removed more intermediate harmonics 337

338 (m = 4, 5, 6), the amplitude of the global m = 3 perturbation is further reduced. Another interesting 339 phenomenon is that after removing the intermediate harmonics in the simulation, the amplitudes of 340 the higher harmonics exhibit an enhancement, examples of which can be seen for the m = 5, 6341 harmonics in Figure 11 (c), and the m = 7 harmonic in Figure 11 (d). By removing the intermediate 342 harmonics, the inward propagation channel from higher harmonics to lower harmonics is stifled, 343 this results in amplitude decline of the inside lower harmonics and flux accumulation at the outside 344 higher harmonics.



Figure 11. The radial structures of $b_{m,n}^r$ in the EAST n = 1 RMP simulation (a) without any specific treatment, (b) employing interpolations and Fourier transformations (all harmonics are retained), (c) artificially removing the m = 4 harmonic, and (d) artificially removing the m = 4, 5, 6 harmonics.



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Figure 12. The distributions of the generalized poloidal angle θ_s of basic straight field line coordinate and the uniformly distributed poloidal angle θ_c .

353 Based on the above results about effects of the poloidal harmonics coupling, it is suggested that, in comparison with the single-harmonic-RMP, the multiple-harmonic-RMP could efficiently 354 drive the development of MHD instabilities in the central plasma region. Therefore, a set of 355 356 simulations is carried out to investigate roles of the multiple-harmonic-RMP on dynamic process of 357 the tearing mode instabilities. The simulations are carried out with the equilibrium shown in Figure 358 7 and the RMPs are applied inside the plasma boundary with the formula of Eq. (7). The multiple-359 harmonic-RMP is implemented by changing the generalized poloidal angle θ_s of the basic straight field line coordinate in Eq. (7) into the uniformly distributed poloidal angle θ_c . Note that magnetic 360 field lines are no longer straight in the $\theta_c - \phi$ plane. The distributions of θ_s and θ_c are shown 361 in Figure 12 (a) and (b), respectively. The RMP with $\delta \psi_{2,1} = 4 \times 10^{-5}$ applied with the θ_s or θ_c 362 dependency produced the radial distributions of the $b_{n=1}^r$ spectra as shown in Figure 13. The RMP 363 depending on θ_s contains only the single m/n = 2/1 harmonic as shown in Figure 13 (a), while the 364 365 latter one with the θ_c dependency contains multiple harmonics ranging from $m = 2 \sim 7$ as shown 366 in Figure 13 (b). Apparently, the multiple-harmonic-RMP with the θ_c dependency creates the 367 multiple harmonic perturbations at the pedestal region, which results in a large enhancement of the non-resonant components (|m| > |nq|) at the q = 2 rational surface due to the successful penetration 368 of high harmonic perturbations. Consequently, the resulted tearing mode response at the q = 2369 rational surface from the multiple-harmonic-RMP is much larger than that from the single-370 harmonic-RMP as shown by Figure 14. 371



Figure 13. The radial distributions of the $b_{n=1}^r$ spectra at $t = 423\tau_A$ for (a) the single-harmonic-RMP and (b) the multiple-harmonic-RMP.



Figure 14. Time evolutions for amplitudes of $b_{m/n=2/1}^r$ with different RMPs: the red squares for the single-harmonic-RMP and the blue circles for the multiple-harmonic-RMP.

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We also find from these present simulations that nonlinear effects on the inward penetration of higher harmonic RMPs are negligible due to the overlap condition $|\partial \zeta_r / \partial r| < 1$ being well satisfied. Concurrently, the linear simulations also give the same results as above. This indicates that the toroidal effect on RMP penetration is associated with the intrinsic symmetry breaking of the toroidal equilibrium magnetic field in the poloidal direction. Nevertheless, nonlinear effects may still be important when the magnetic islands grow large enough to affect the adjacent rational surfaces.

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388 5 Conclusion and discussion

In the present paper, the CLTx code is used to study the n = 1 RMP penetration. The comparison study between linear and nonlinear modeling finds that with the presence of toroidal plasma rotation, the final steady state or saturated state for high resonant harmonics could be obtained in the initial 392 value simulations of the CLTx code using the linearized MHD equations only. With this being the 393 case, nonlinear effects are negligible since the magnetic islands evolve into a linearly saturated state due to plasma response and shielding. Therefore, the nonlinear simulations for discharge 52340 give 394 395 the same results for rational surfaces around the pedestal as the linear results calculated by the 396 MARS-F code [10, 20] and the linearized CLTx code [18]. However, without toroidal rotation, the linear MHD modeling performed by the CLTx code breaks down. This is because, without plasma 397 398 rotation and nonlinear effects, the inside resonant harmonics in purely linear simulations give 399 evolution dynamics with continuous growth where the final saturated state is not obtained unless 400 the nonlinear terms are included. Consequently, this leads to the failure of predicting the shielding 401 effect by plasma response. Therefore, for future Tokamaks with zero or low-speed toroidal rotation, 402 such as ITER [39], the inclusion of nonlinear effects in the CLTx code will be necessary.

403 The simulations focusing on the toroidal effect in RMP penetration demonstrate that poloidal 404 harmonics coupling [6, 30] is a consequence of the toroidal effect instead of nonlinear effects. With 405 low resistivity, the single-harmonic-RMP is hard to penetrate the mode-rational surface because of 406 the plasma screening effect, resulting in a truncation on the radial mode structure. On the other hand, 407 the non-resonant components in the multiple-harmonic-RMP could avoid the plasma shielding, and thus play an effective role in the RMP penetration through the poloidal harmonics coupling. 408 409 Consequently, with the inclusion of higher harmonics in RMP, the penetration by lower harmonics 410 could become larger. The removal of the intermediate harmonics prevents the inward penetration of 411 the outside higher harmonics, which results in an amplitude decrease (increase) of the inner lower (outer higher) harmonics. Finally, the observed mode coupling is mainly caused by the 412 inhomogeneity of the toroidal equilibrium magnetic field rather than from nonlinear mode coupling. 413 414 Consequently, nonlinear effects are unimportant for mode coupling when the toroidal effect 415 dominates. This indicates a possible explanation for the similar results obtained by both the linear 416 and nonlinear simulations.

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