Drift Alfvén Energetic Particle Stability with Circulating Particles 1 2 Y. Li¹, S. Hu², W. Zheng³, Y. Xiao^{1*} 3 ¹ Institute for Fusion Theory and Simulation and Department of Physics, Zhejiang University, 4 Hangzhou, 310027, PRC 5 ² College of Physics, Guizhou University, Guiyang, PRC 6 ³ Academy of Mathematics and Systems Science, Chinese Academy of Sciences 7 * (Corresponding author) E-mail: yxiao@zju.edu.cn 8 9 Abstract 10 11 We develop from scratch a comprehensive linear stability eigenvalue code based on finite element method (FEM), namely the Drift Alfvén Energetic Particle Stability 12 (DAEPS) code, to investigate the most unstable or stable dangerous modes widely 13 observed in toroidal fusion plasmas. The DAEPS code is dedicated to providing a 14 15 thorough understanding of marginally unstable low frequency mode physics in collisionless plasmas, e.g., shear Alfvén wave (SAW) and drift Alfvén wave (DAW) 16 physics with energetic particle (EP) effect. DAEPS can calculate the linear frequency 17 and growth rate for these modes by keeping correct asymptotic behavior in ballooning 18 19 space. In this work, we demonstrate that the DAEPS code is able to analyze linear electromagnetic modes excited by circulating particles, including thermal particle 20 excited BAE and EP excited TAE which are successfully benchmarked with other codes 21 and theories, where the finite orbit width is discovered to play an important stabilizing 22 23 role which are usually ignored by traditional theory.

24

25 I. Introduction

Tokamak experiments observe that energetic particles (EPs) can resonantly destabilize various Alfvén eigenmodes (AEs) [1-6]. These Alfvénic fluctuations, which are marginally unstable or weakly damped in the presence of EP, have been shown to eject a large number of resonant EPs from the core plasma [1, 3, 5, 7]. These observed

Alfvénic fluctuations are caused by various instabilities excited by EPs, which consist 30 of beta-induced Alfvén eigenmode (BAE) [8], toroidicity-induced Alfvén eigenmode 31 32 (TAE) [9], energetic particle mode (EPM) [10], reversed shear Alfvén eigenmode (RSAE) [11], etc. Some of these instabilities are primarily related to the parallel 33 dynamics of circulating EPs [12], while some are related to the precessional dynamics 34 35 of trapped EPs [13]. The EP heat and particle loss caused by these Alfvén eigenmodes will pose a grand challenge for approaching and sustaining the ignition condition for 36 future fusion reactors including ITER, as well as a stringent constraint for the lifetime 37 of the wall material that is bombarded continuously by this high power EP flux [12, 14]. 38 39 Therefore, it is important to fully understand the AE physics and develop effective methods to regulate the AE induced EP transport. 40

In the last decades, lots of theoretical [9, 15-17] efforts have been made to 41 understand the AE physics. The linear and nonlinear properties of AEs have also been 42 widely studied by the numerical simulation using MHD-kinetic hybrid codes [3, 18-22] 43 and gyrokinetic codes [4, 6, 23, 24]. In the numerical investigation of the Alfvénic 44 45 instabilities, the ballooning representation is widely employed by various numerical codes [7, 25-28]. However, the boundary condition (BC) implemented in these 46 numerical codes usually set the fluctuating field $\delta \psi \rightarrow 0$ as the extended poloidal 47 angle of the ballooning representation in the computational boundary [7, 25-28], which 48 cannot accurately represent the asymptotic behavior of the mode structure for most 49 interesting cases. The inaccuracy of the asymptotic behavior will cause even larger 50 51 errors in calculating frequency and growth rate for marginally unstable or damping modes, and large deviations from the actual mode structure in the inertial region. Thus, 52 the unphysical boundary conditions implemented in the numerical codes will lead to 53 inaccuracy in computing the potential energy and misinterpretation of the AE physics. 54

The hybrid MHD-kinetic model extensively used to study EP induced Alfvénic instabilities consists of two approaches, namely perturbative approach and nonperturbative approach [21]. In the perturbative approach, the eigen frequency and the mode structure are calculated from the MHD equation, which are then used to calculate the kinetic response and the kinetic potential energy δW_k . This kinetic energy transferring from the EP to the mode is then used to calculate the linear growth rate. Another approach, the non-perturbative approach includes the EP contribution through the plasma pressure or current perturbation, whose mode structure and eigen frequency differ from those from the MHD equation in many important circumstances. The perturbative approach cannot be applied to the EPM, since the mode doesn't exist in the MHD framework and is very sensitive to the EP source [10, 29].

In this paper, we develop a non-perturbative eigenvalue code called Drift Alfvén Energetic Particle Stability code, which uses the finite element method (FEM) to selfconsistently solve the eigen frequency and growth rate, as well as the asymptotic behavior in the inertial region. This code is benchmarked on various instabilities involving circulating particle dynamics with other codes and theories. The importance of the finite Larmor radius effect (FLR) and finite orbit width effect (FOW) is discovered in the code verification process.

The paper is organized as follows. In Section II, we introduce the model equations of the DAEPS code. In Section III, the numerical method used in DAEPS is discussed in details. Then we use the DAEPS to study the linear physics of BAE/KBM and benchmark these physics issues with other codes and theories in Section IV. In Section V, we calculate the linear properties of the EP excited TAE using DAEPS. In the last section, we give a brief summary of the current DAEPS development status and discuss the future work.

80

81 II. DAEPS Model Equations

The model equations for the Drift Alfvén Energetic Particle Stability code (DAEPS code) are originated from the general fishbone-like dispersion relation (GFLDR) [29, 30]. The theoretical framework of GFLDR can be used to analyze SAW/DAW physics by adopting the mode structure decomposition (MSD) method [31] and asymptotic matching between the inertial region/singular layer and the ideal region [15]. The GFLDR, for a single *n* toroidal mode, takes the form of $i|s|\Lambda_n = \delta \hat{W}_{nf} + \delta \hat{W}_{nk}$, where

the generalized inertial term Λ_n is the normalized singular layer contribution 88 including kinetic response, s is the magnetic shear, $\delta \hat{W}_{nf}$ and $\delta \hat{W}_{nk}$ are the fluid 89 and kinetic contributions of the potential energy, respectively. The dispersion relation 90 can be formulated in a quadratic form due to the variational nature of GFLDR. A trial 91 function is needed to calculate the frequency, growth rate, fluid and kinetic potential 92 energies and their asymptotic behaviors, which needs to be accurate enough in the 93 asymptotic limit for a precise calculation of the linear eigenvalues. For high toroidal 94 mode number n, when radial envelope variation can be ignored in the lowest order, 95 GFLDR becomes the local dispersion relation $i\Lambda_n = \delta \overline{W}_{nf} + \delta \overline{W}_{nk}$, where 96 $\delta \overline{W}_n = \delta \hat{W}_n / |s|$ for localized modes. 97

The mode structure decomposition [31] is valid for general toroidal mode number n, which introduces the projection operator transforming the fluctuation function ffrom real space $f(r, \theta, \zeta)$ to the mode structure decomposition (MSD) space $\hat{f}_n(r, \theta)$, i.e., $\mathcal{P}_{Bn}: f(r, \theta, \zeta) \mapsto \hat{f}_n(r, \theta)$, which takes the form of :

102
$$f(r,\theta,\zeta) = \sum_{m} e^{in\zeta - im\theta} \int e^{i(m-nq)\vartheta} \mathcal{P}_{Bn}(r,\vartheta) [f] d\vartheta \quad , \tag{1}$$

103 where \mathcal{P}_{Bn} is the function mapping between the two spaces. For high *n* mode with 104 moderate to high magnetic shear, the unstable modes are localized around the mode 105 rational surface, the envelope variation is weak, and the MSD can be reduced to the 106 ballooning representation [31]:

107
$$f(r,\theta,\zeta) = \sum_{n,m} A_n(r) e^{in\zeta - im\theta} \int e^{i(m-nq)\vartheta} \mathcal{P}_{Bn}(r,\vartheta) [f_{0n}] d\vartheta \quad , \tag{2}$$

where the fluctuation function f shows a two-scale feature in the radial structure with f_{0n} varying in the micro-scale $\Delta_0 = (nq')^{-1}$ and macro-scale O(a), and the envelope function $A_n(r)$ varying in the meso-scale $(\Delta_0 a)^{1/2}$ which can be further described by an eikonal ansatz $A_n(r) \sim \exp\left[i\int nq' \vartheta_k(r)dr\right]$. 112 The DAEPS model equations assume the gyrokinetic ordering and solve the 113 gyrokinetic-Maxwell system by singling out essential kinetic physics. The tearing mode 114 physics is ignored, so the perturbed parallel vector potential δA_{\parallel} can be described by 115 a magnetic scalar potential $\delta \psi$ with $\partial_t \delta A_{\parallel} = -c \partial_{\parallel} \delta \psi$. Using the s- α equilibrium 116 model, the following vorticity equation is solved in the DAEPS model [32]:

$$117 \qquad B\partial_{\parallel} \left[\frac{1}{B} \frac{k_{\perp}^2}{k_{\theta}^2} \partial_{\parallel} \right] \delta\psi + \frac{\omega \left(\omega - \omega_{*pi} \right)}{v_A^2} \frac{k_{\perp}^2}{k_{\theta}^2} \delta\phi + \frac{\alpha}{q^2 R^2} g \,\delta\psi = \sum_j \left\langle \frac{4\pi q_j}{k_{\theta}^2 c^2} J_0 \omega \omega_{dj} \delta K_j \right\rangle_{\nu}, \quad (3)$$

118 where the left hand side (LHS) is the fluid contribution, consisting of field line bending, 119 inertial and ballooning interchange, and the right hand side (RHS) is the kinetic 120 compression, which could come from either energetic particles or thermal particle. 121 $\alpha = -Rq^2\beta'$ with $\beta = 8\pi P/B^2$ is the dimensionless pressure gradient that provides

122 instability drive,
$$k_{\theta} = \frac{nq}{r}$$
, $\omega_{*pi} = \frac{\mathbf{k} \times \mathbf{b}}{\Omega_{ci} m_i} \cdot \nabla P_i$ is the ion diamagnetic frequency,

123
$$\omega_{dj} = \mathbf{b} \times \left(\mu \nabla B + v_{\parallel}^2 \mathbf{\kappa}\right) / \Omega_{cj}$$
 is the drift frequency for the particle species j , q is the
124 safety factor, the q_j is the charge for the particle species j , and $\langle \cdots \rangle_{v} = \int (\cdots) d^3 \mathbf{v}$

125 denotes integration over the velocity space, $v_A = \frac{B}{\sqrt{4\pi nm}}$ is the Alfvén velocity,

126 $J_0 = J_0(k_{\perp}\rho_j)$ is the Bessel function of the first kind of zeroth order, $\rho_j = v_{\perp} / \Omega_{cj}$ is 127 the Larmor radius with Ω_{cj} the cyclotron frequency, $k_{\perp}^2 = k_{\theta}^2 \kappa_{\perp}^2$ with

128
$$\kappa_{\perp}^2 = 1 + (s\theta - \alpha \sin\theta)^2$$
 and $g = \cos\theta - (s\theta - \alpha \sin\theta)\sin\theta$, $\partial_{\parallel} = \frac{\mathbf{B}}{B} \cdot \nabla = \frac{1}{qR} \partial_{\theta}$, and

129 θ is the extended poloidal angle in the cover space of the ballooning representation.

The fluid contribution of energetic particles is assumed negligible. The ideal MHD approximation $\delta E_{\parallel} = \partial_{\parallel} \delta \phi - c^{-1} \partial_t \delta A_{\parallel} = 0$ is used for convenience to give $\delta \phi = \delta \psi$, which is valid for linear physics of BAE and EP excited TAE [9, 32], and thus the quasineutrality condition is no longer necessary. For most relevant cases we consider high *n* modes, thus in the ballooning representation the vorticity equation of Eq. (3) can be 135 written explicitly as [32, 34]:

136
$$\partial_{\theta}k_{\perp}^{2}\partial_{\theta}\delta\psi + \frac{\omega(\omega - \omega_{*pi})}{\omega_{A}^{2}}k_{\perp}^{2}\delta\psi + \alpha g\delta\psi = \sum_{j}\left\langle\frac{4\pi q_{j}q^{2}R^{2}}{c^{2}}J_{0}\left(k_{\perp}\rho_{j}\right)\omega\omega_{dj}\delta K_{j}\right\rangle_{v}.$$
 (4)

137 In Eq. (4), ω_A is the Alfvén frequency with $\omega_A^2 = \left(\frac{v_A}{qR}\right)^2 = \omega_{A0}^2 \left(1 - 4\epsilon \cos\theta\right)$ for a

138 large aspect ratio with circular flux surface tokamak with $\epsilon = r / R$, where ω_{A0} is the 139 Alfvén frequency on the magnetic axis that determines the basic characteristic time 140 scale for Eq. (4).

141 The gyrocenter distribution function δK_j can be solved through the linearized 142 collisionless electromagnetic gyrokinetic equation:

143
$$\left(\frac{v_{\parallel}}{qR}\partial_{\theta} - i\omega + i\omega_{dj}\right)\delta K_{j} = i\frac{q_{j}}{m_{j}}QF_{0j}\frac{\omega_{dj}}{\omega}J_{0}\left(k_{\perp}\rho_{j}\right)\delta\psi \quad , \tag{5}$$

144 where $QF_{0j} = (\omega \partial_E + \hat{\omega}_{*j})F_{0j}$ is the free energy provided by the phase space gradient 145 of the equilibrium distribution function F_{0j} , with $E = \frac{1}{2}v^2$ and $\hat{\omega}_{*j} = \Omega_{cj}^{-1}\mathbf{k} \times \mathbf{b} \cdot \nabla$.

The asymptotic behavior of $\delta \psi$ as $\theta \to \pm \infty$, which is critical for calculating the eigen frequency and growth rate and identifying whether a mode is physical or spurious, is determined by the outgoing wave boundary condition with causality constraints. In order to properly handle the asymptotic behavior, the vorticity equation should be written as the Schrödinger-like form:

151
$$\left[\partial_{\theta}^{2} + \frac{\omega(\omega - \omega_{*pi})}{\omega_{A}^{2}} + V(\theta)\right]\Psi = \sum_{j} \left\langle \frac{4\pi q_{j} q^{2} R^{2}}{k_{\theta}^{2} c^{2} \kappa_{\perp}} J_{0} \omega \omega_{dj} \delta K_{j} \right\rangle_{v} , \qquad (6)$$

152 where $V(\theta) = \kappa_{\perp}^{-2} \alpha \cos \theta - \kappa_{\perp}^{-4} (s - \alpha \cos \theta)^2$ is the effective potential well, and 153 $\Psi = \kappa_{\perp} \delta \psi$ is the perturbed magnetic scalar potential, whose asymptotic behavior can 154 be derived by taking the limit $\theta \to \pm \infty$. Ignoring the variation of magnetic field along 155 the field line, the asymptotic behavior will be described by a wave equation:

156 $\left(\partial_{\theta}^{2} + \Lambda^{2}\right)\Psi = 0.$ (7)

157 Employing the outgoing wave boundary condition, the asymptotic behavior of the

158 perturbed magnetic scalar potential takes the form of:

159

$$\lim_{\theta \to \pm \infty} \Psi = e^{i\Lambda |\theta|} \quad , \tag{8}$$

where Λ is the inertial term in the GFLDR [15, 29, 30], which contains the kinetic contribution. The continuous spectrum corresponds to purely real Λ , while the discrete spectrum corresponds to purely imaginary Λ [32].

163 Considering the periodic variation in ω_A along the field line due to the periodicity 164 of magnetic field, the asymptotic behavior of Ψ can be expressed in the following 165 form using the Floquet theory [30, 35]:

166
$$\lim_{\theta \to \pm \infty} \Psi = e^{i\nu|\theta|} P(\theta), \tag{9}$$

167 where $P(\theta)$ is a 2π -periodic function. The causality constraint requires $\operatorname{Re} v > 0$ 168 for the outgoing wave boundary condition.

169 The RHS of Eq. (6) involves the integration of perturbed gyrocenter distribution 170 function δK_j , which can be solved from Eq. (5). Considering only the circulating 171 particle response, the gyrokinetic equation can be integrated directly in the ballooning 172 space [26-28] as:

173

$$\delta K_{j}(\theta, \hat{\sigma}, \lambda, E) = \int_{\theta}^{-\hat{\sigma} \cdot \infty} \exp\left[i \operatorname{sign}\left(\operatorname{Im} \omega\right) \int_{\theta}^{x} qR \frac{-\omega + \omega_{dj}(y)}{|v_{\parallel}|} dy\right] \\ \times (-\hat{\sigma}) i \frac{q_{j}}{m_{j}} \frac{qR}{|v_{\parallel}|} QF_{0j} \frac{\omega_{dj}(x)}{\omega} J_{0} \frac{\Psi(x)}{\kappa_{\perp}(x)} dx \qquad (10)$$

174 where $\hat{\sigma} = \frac{v_{\parallel}}{|v_{\parallel}|}$ is the direction of parallel velocity, $\lambda = \frac{\mu B_0}{E}$ is the velocity pitch

angle, and the signum function of the imaginary part of ω is the causality constraint to avoid the integral divergence. Hence, the kinetic compression term (KC) can be written as:

$$\begin{aligned} \text{KC} &= \kappa_{\perp}^{-1} \left\langle \frac{4\pi q_{j} q^{2} R^{2}}{k_{\theta}^{2} c^{2}} \omega \omega_{dj} J_{0} \delta K_{j} \right\rangle_{v} \\ &= \frac{4\pi q_{j} q^{2} R^{2}}{k_{\theta}^{2} c^{2}} \int_{0}^{\infty} dE \int_{0}^{1} d\lambda \int_{-\infty}^{\infty} dx \frac{2\pi E}{|v_{\parallel}|} \frac{\omega_{dj}(\theta)}{\kappa_{\perp}(\theta)} J_{0} i \frac{q_{j}}{m_{j}} \frac{qR}{|v_{\parallel}|} QF_{0j} \quad . \end{aligned}$$
(11)
$$\times \exp \left[i \text{sign} \left(\text{Im} \, \omega(\theta - x) \right) \int_{\theta}^{x} dy \frac{-\omega + \omega_{dj}}{|v_{\parallel}|} qR \right] \frac{\omega_{dj}(x)}{\kappa_{\perp}(x)} J_{0} \Psi(x) \end{aligned}$$

Thus, the DAEPS model equation becomes an integral-differential equation that manifests itself a nonlinear eigenvalue problem. Appropriate numerical method needs to be found to solve this equation, as shown in the next section.

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183 III. Numerical Method

The DAEPS code uses the finite element method with cubic B-Spline to solve Eq. (6) with special elements near boundaries [36]. For total N grid points in the extended poloidal angle domain with equal grid step h, the finite element basis function $|n\rangle, (2 \le n \le N-2)$, lies in region (n-2)h < x < (n+2)h, and takes the form of:

188
$$|n\rangle = \phi\left(\frac{x}{h} - n\right)$$
, (12)

189 where $\phi(x)$ is a piecewise function:

190
$$\phi(x) = \begin{cases} \frac{4}{3} + 2x + x^2 + \frac{x^3}{6} & -2 \le x < -1 \\ \frac{2}{3} - x^2 - \frac{x^3}{2} & -1 \le x < 0 \\ \frac{2}{3} - x^2 + \frac{x^3}{2} & 0 \le x < 1 \\ \frac{4}{3} - 2x + x^2 - \frac{x^3}{6} & 1 \le x \le 2 \end{cases}$$
(13)

For the special elements near the left boundary $x = x_L$, the boundary elements $|-1\rangle$, $|0\rangle$ and $|1\rangle$ take the form of:

$$|-1\rangle(hy+x_{L}) = 1-3y+3y^{2}-y^{3} \qquad 0 \le y \le 1$$

$$|0\rangle(hy+x_{L}) = \begin{cases} y-\frac{3}{2}y^{2}+\frac{7}{12}y^{3} & 0 \le y < 1\\ \frac{2}{3}-y+\frac{1}{2}y^{2}-\frac{1}{12}y^{3} & 1 \le y \le 2 \end{cases}$$

$$|1\rangle(hy+x_{L}) = \begin{cases} \frac{1}{2}y^{2}-\frac{11}{36}y^{3} & 0 \le y < 1\\ -\frac{1}{2}+\frac{3}{2}y-y^{2}+\frac{7}{36}y^{3} & 1 \le y < 2\\ \frac{3}{2}-\frac{3}{2}y+\frac{1}{2}y^{2}-\frac{1}{18}y^{3} & 2 \le y \le 3 \end{cases}$$

(14)

As shown in the Fig. 1, these special elements near the boundaries have their special properties, where $|-1\rangle$ has non-zero value at the boundary, while $|-1\rangle$ and $|0\rangle$ have non-zero derivatives at the left boundary. These properties particularly favor Dirichlet and Neumann boundary condition.



198

199 Figure 1: The B-Spline finite element with N = 6 grid within the interval $[x_L, x_R]$.

The perturbed magnetic scalar potential in Eq. (6) can be expressed by a linear combination of the finite elements $|n\rangle$, i.e., $\Psi(\theta) = \sum_{n=-1}^{N+1} a_n |n\rangle(\theta)$. Hence, the weak

form of Eq. (6) takes the form of:

203
$$\sum_{n=-1}^{N+1} a_n \langle m | \mathrm{KC} | n \rangle = \sum_{n=-1}^{N+1} a_n \left[-\left(\partial_\theta | m \rangle\right)^{\dagger} \partial_\theta | n \rangle + \langle m | \partial_\theta | n \rangle_{\theta_-}^{\theta_+} + \langle m | \frac{\omega \left(\omega - \omega_{*p_i}\right)}{\omega_A^2} + V(\theta) | n \rangle \right], \quad (15)$$

where the computational domain is taken as $[\theta_-, \theta_+]$, and the boundary condition term

205 $\langle m | \partial_{\theta} | n \rangle$, considering the Neumann boundary condition $\partial_{\theta} \Psi |_{\theta \to \theta_{\pm}} = \pm i \Lambda \Psi$, can be 206 transformed to:

207
$$\langle m | \partial_{\theta} | n \rangle_{\theta_{-}}^{\theta_{+}} = i \Lambda [\langle m | n \rangle (\theta_{+}) + \langle m | n \rangle (\theta_{-})].$$
 (16)

Such a boundary condition is essentially an absorbing boundary condition for 208 outgoing wave with no reflection for given asymptotic behavior, which is important for 209 the causality constraint. The self-adjointness of the LHS of Eq. (6) requires that the 210 eigenfunctions appear in complex conjugate pairs in the ideal MHD limit, where the 211 eigenmode structure Ψ and its complex conjugate Ψ^* are both eigenfunctions with 212 the same eigenvalue, and with opposite signs for the real part of the asymptotic 213 parameter Λ , which denote two opposite propagation directions for the wave. The 214 causality constraint $Re\Lambda > 0$ suggests that there should exist only one physical 215 solution in each pair of solutions [29]. However, with improper boundary condition that 216 reflects the outgoing wave backwards, the calculated mode structure Ψ is 217 superimposed by the unphysical reflected mode Ψ^* , which leads to the inaccuracy in 218 the eigenfunction and the corresponding eigenvalue. 219

The FEM weak form of Eq. (6), as shown in Eq. (15), is closely related to the 220 GFLDR framework [29, 30]. By multiplying the complex conjugate of FEM coefficient 221 a_n^{\dagger} and performing the summation over the FEM space, the left hand side (LHS) of Eq. 222 (15) is the local kinetic contribution to the potential energy $\delta \overline{W}_k$. The non-boundary 223 terms in the right hand side (RHS) are the local fluid contribution to the potential energy 224 $\delta \overline{W}_{f}$, and the boundary term is the inertial term in GFLDR. Since the computational 225 domain should include the ideal region $\theta \ll 1$, the boundary condition Eq. (16) at 226 computational boundary θ_{\pm} is essentially performing the asymptotic matching for Ψ 227 from the ideal region to the inertial region, i.e., $\Psi_{ID}^{\dagger}\partial_{\theta}\Psi_{ID}|_{-\infty}^{+\infty} = \Psi_{IN}^{\dagger}\partial_{\theta}\Psi_{IN}|_{-0}^{+0} = 2i\Lambda$, 228 which suggests that the computational domain should be large enough to cover the 229 inertial region. Using the DAEPS model, both fluid and kinetic contributions to the 230 potential energy and singular layer can be accurately calculated, and the solution to the 231

FEM weak form of DAEPS equation can automatically satisfy the GFLDR equation. Using the FEM, the matrix form of the vorticity equation Eq. (15) becomes a nonlinear eigenvalue equation: $\vec{A}(\Lambda, \omega)\mathbf{x} + \omega \vec{B}\mathbf{x} + \vec{C}\mathbf{x} = 0$. Here an iterative algorithm is designed to solve the eigen frequency ω and the asymptotic behavior of the mode structure Λ , where ω is calculated from the eigenvalue of the matrix, the asymptotic behavior is fitted from the eigenvector of the matrix, and both of them are reserved for next iteration until the convergence is achieved.

We note that the kinetic compression term KC, on the LHS of Eq. (15), involves amultidimensional integration:

$$\sum_{n=-1}^{N+1} a_n \langle m | \mathrm{KC} | n \rangle = \frac{4\pi q_j q^2 R^2}{k_\theta^2 c^2} \sum_{n=-1}^{N+1} \int_{-\infty}^{\infty} d\theta \int_0^{\infty} dE \int_0^1 d\lambda \int_{-\infty}^{\infty} dx \frac{2\pi E}{|v_{\parallel}|} \frac{\omega_{dj}(\theta)}{\kappa_{\perp}(\theta)} J_0$$

$$\times i \frac{q_j}{m_j} \frac{qR}{|v_{\parallel}|} QF_{0j} \langle m | (\theta) \frac{\omega_{dj}(x)}{\kappa_{\perp}(x)} J_0 a_n | n \rangle (x) \qquad , (17)$$

$$\times \exp \left[i \mathrm{sign} \left(\mathrm{Im} \, \omega (\theta - x) \right) \int_{\theta}^x dy \frac{-\omega + \omega_{dj}}{|v_{\parallel}|} qR \right]$$

where we use the numerical method of global h-adaptive multidimensional integration over hypercube [37, 38] to calculate the KC term, and piecewise Gauss-Legendre quadrature to calculate the FEM integral.

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246 IV. BAE/KBM with Kinetic Thermal Ions

Beta-induced Alfvén eigenmode (BAE) exists in the finite pressure induced gap for the Alfvén continuum, which is caused by the coupling between SAW and sound wave (SW) induced by plasma compressibility [8, 12]. BAE can be excited by the plasma compressibility from either thermal ions or energetic particles via wave-particle resonance [32].

For simplicity, here we only consider the BAE excited by the circulating thermal particles. Since the BAE is a $k_{\parallel} \approx 0$ mode, the mode structure of BAE in the ballooning representation varies slowly with the extended poloidal angle θ in the inertial region, which means the real part of asymptotic behavior ReA is small [6]. Hence BAE is a long wavelength mode, $\Lambda \sim q\sqrt{\beta}$, the ideal MHD assumption of neglecting parallel electric field holds, $\delta E_{\parallel} \approx 0$, [6], since BAE propagates in the ion diamagnetic direction [32]. The KC term in Eq. (17) can be simplified using the drift center transformation. By expanding the pull-back operator $\exp(-ik_{\perp}\rho_{dj}\cos\theta)$ to the lowest order [10, 34] and performing scale separation between the fast variation $\theta_0 \sim O(1)$ and slow variation $\theta_1 \gg 1$, the reduced kinetic compression term takes the form of:

264 where $\omega_{ij} = \frac{|v_{||}|}{qR}$ is the transit frequency, $J_1 = J_1(k_{\perp}\rho_{dj})$ is the Bessel function of the

265 first kind of first order, and $\rho_{dj} = \frac{\Omega_{dj}}{k_{\theta}\omega_{ij}}$ is the drift-orbit width with $\Omega_{dj} = \omega_{dj} / g$. The

term $(\omega_{ij}^2 - \omega^2)^{-1}$ is identified as the transit resonant interaction between particle and wave. Ignoring the FOW and FLR effects, the kinetic compression term in Eq. (11) can also be further simplified by assuming the aforementioned scale separation:

It is known that the BAE branch can be coupled with kinetic ballooning mode (KBM) branch in some parameter regime [32]. Here for the code benchmark purpose, we first choose the KBM instability, which is also a small k_{\parallel} mode, excited by only thermal ions. Fig. 2(a) shows the comparison of the real frequency and growth rate between DAEPS and the initial value linear gyrokinetic PIC code AWECS [25], with the prescribed plasma parameters q = 1.2, magnetic shear s = 0.4, $\epsilon_{ni} = L_{ni} / R = 0.175$,

276 with
$$L_{ni} = -\partial_r \ln n_i$$
, $\eta_i = \frac{d \ln T_i}{d \ln n_i} = 2$. In Fig 2(a), the solid line and dashed line show

277 the eigen frequency and growth rate vs. the dimensionless pressure gradient α

respectively, the blue squares are from DAEPS with reduced KC, the red triangles are 278 from DAEPS with complete KC, and the black circles are from the AWECS result. The 279 DAEPS result is fully consistent with the AWECS result. In addition, we note that the 280 difference in the linear frequency, growth rate and asymptotic behavior is less than 10% 281 between the reduced KC and complete KC, as shown by Fig. 2(a) & (b). The small 282 differences between DAEPS and AWECS can be attributed to the ion polarization and 283 parallel electric field ignored in the DAEPS model for simplicity. The comparison of 284 285 the KBM eigenvalue and asymptotic behavior suggests that using the reduced form of KC in the DAEPS code can accelerate the calculation of the eigenvalue and asymptotic 286 behavior without losing accuracy to a speed dozens of times faster than using the 287 complete KC term by substantially reducing numerical integration time. 288



289 290



Figure 2: Comparison of linear dispersion and eigenmode asymptotic behavior for KBM between the DAEPS results with complete KC term (cKC) and reduced KC term (rKC).(a) real frequency ω_r and growth rate γ vs α ; (b) asymptotic behavior Λ vs α .

297 Next we show the benchmark for the BAE instability. According to the GFLDR 298 theory, the BAE dispersion relation, after assuming $\omega \sim \omega_{ti} \sim \omega_{*pi} \ll \omega_A$, is given by 299 the following equation [32]:

$$300 \quad \left\{\frac{\omega(\omega-\omega_{*pi})}{\omega_{A}^{2}}+q^{2}\frac{\omega_{ii}}{\omega_{A}^{2}}\left[\left(\omega-\omega_{*ni}\right)F\left(\frac{\omega}{\omega_{Ti}}\right)-\omega_{*Ti}G\left(\frac{\omega}{\omega_{Ti}}\right)-\frac{N^{2}\left(\omega/\omega_{Ti}\right)}{D\left(\omega/\omega_{Ti}\right)}\right]\right\}^{1/2}=\Lambda, \quad (20)$$

301 where $\omega_{Ti} = \sqrt{\frac{2T_i}{m_i}} \frac{1}{qR}$, and the functions, F(x), G(x), N(x) and D(x) are

302 introduced by Ref. [32]:

$$N(x) = \left(1 - \frac{\omega_{*ni}}{\omega}\right) \left[x + \left(\frac{1}{2} + x^{2}\right)Z(x)\right] - \frac{\omega_{*Ti}}{\omega} \left[x\left(\frac{1}{2} + x^{2}\right) + \left(\frac{1}{4} + x^{4}\right)Z(x)\right]$$
$$D(x) = \frac{1}{x} \left(1 + \frac{1}{\tau}\right) + \left(1 - \frac{\omega_{*ni}}{\omega}\right)Z(x) - \frac{\omega_{*Ti}}{\omega} \left[x\left(\frac{1}{2} + x^{2}\right) + \left(\frac{1}{4} + x^{4}\right)Z(x)\right]$$
$$F(x) = x \left(x^{2} + \frac{3}{2}\right) + \left(x^{4} + x^{2} + \frac{1}{2}\right)Z(x)$$
$$G(x) = x \left(x^{4} + x^{2} + 2\right) + \left(x^{6} + \frac{x^{4}}{2} + x^{2} + \frac{3}{4}\right)Z(x)$$
$$. (21)$$

According to the theory, there exists a critical value for η_i , below which the KBM 304 branch is the most unstable branch, and above which the coupled BAE and KBM branch 305 is the most unstable branch. In order to better estimate the value of Λ in the theory, 306 307 the asymptotic behavior value Λ calculated by the DAEPS code is substituted back into the Eq. (20) to compute the linear frequency and growth rate. An example is shown 308 in Fig. 3 with the plasma parameters $\beta_i = 0.01$, q = 1.5, $\omega_{*_{ni}} = \omega_{ii}$, and $\eta_i > 0.5$ is 309 above the critical value, which ensures that the mode calculated by DAEPS stays in the 310 311 coupled BAE/KBM branch, where the red triangles and diamonds are from the DAEPS code with complete KC term (cKC) and reduced KC term (rKC) respectively, and the 312 blue circles and squares are from theory given by Eq. (20) with complete KC term (cKC) 313 and reduced KC term (rKC) respectively. As shown in Fig. 3(a), the increasing trend of 314 eigen frequency and growth rate with increasing η_i calculated by the DAEPS code is 315 qualitatively consistent with the theory for both complete KC and reduced KC case. 316 The notable shift between DAEPS and theory in Fig. 3(a) is presumably caused by the 317 FOW and FLR effects, which are treated as higher order and neglected in the 318 conventional theory [32]. To verify this conjecture, we compare the DAEPS results 319 320 using the reduced KC ignoring the FLR and FOW effects in Eq. (19) with the conventional theory in Eq. (20) on the BAE/KBM instability. As shown in Fig. 3(b), 321 the difference in the eigen frequency, growth rate and asymptotic behavior is negligibly 322 small between DAEPS and theory, and the discrepancy is actually less than 10% 323 between DAEPS result using reduced KC term and using complete KC term, which 324 proves that the large discrepancy between DAEPS and theory in Fig. 3(a) is due to the 325

FOW and FLR effects and also verifies the validity of using the reduced KC term in the DAEPS code to accelerate computation. The comparisons in Figs. 3(a) & (b) also demonstrate the stabilizing nature of the FLR and FOW effects in the BAE excitation. The conventional theory overestimates the BAE instability threshold and gives a much larger linear grow rate close to marginal stability, which would affect the nonlinear physics profoundly, especially comparing to experiments.

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Figure 3: Comparison of real frequency ω_r and growth rate γ from the DAEPS code and theory for various η_i : (a) eigenvalue comparison with FLR and FOW effects; (b) eigenvalue comparison without FLR and FOW effects.

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The asymptotic behavior is crucial to solve the eigen frequency and growth rate 339 340 when the mode structure in the inertial region is more important than in the ideal region, which often occurs for the marginally unstable or damping modes, as well as for the 341 342 continuous spectrum located only in the inertial region, such as the Alfvén continuous spectrum to be introduced in the next section. Since BAE/KBM mode is strongly MHD 343 unstable, the asymptotic behavior is not crucial for calculating the eigen frequency and 344 345 growth rate of BAE/KBM. However, the computation cost is substantially reduced with 346 the proper boundary condition since much narrower computational domain is needed, as is demonstrated by following. Here we use the BAE/KBM typical parameters with 347

 $\eta_i = 0.7$ in the preceding study to perform a comparison between the cases with and 348 without the proper boundary condition for the correct asymptotic behavior, where the 349 case without the proper boundary condition is calculated by using the free boundary 350 condition $\partial_{\theta} \Psi = 0$. Fig. 4(a) shows the comparison of the mode structures with 351 different boundary conditions, where the red solid line and the blue dashed line are the 352 real and imaginary parts of the mode structure with the proper BC, while the red circles 353 and blue diamonds are the real and imaginary parts of the mode structure without the 354 proper BC. As is shown in the Fig. 4(a), the difference between these two different BC 355 cases becomes significant in the inertial region, where the logarithm of the mode 356 structure should be described by the linear relationship $\log \Psi = i\Lambda |\theta| + \text{const}$ as is 357 required by the correct asymptotic behavior. A large discrepancy occurs in the inertial 358 region for the logarithm of the mode structure without the proper BC when fitting with 359 the linear relation, as shown in Figs. 4(b) & (c), where the black dotted line is the linear 360 fitting of the logarithm of the mode structure with the proper BC; the red solid line and 361 red circles are the real part of the logarithm of mode structure with and without the 362 proper BC, respectively; and blue dashed line and blue diamonds are the imaginary part 363 of the logarithm of mode structure with and without the proper BC, respectively. 364





Figure 4: Comparison of the mode structures with $\eta_i = 0.7$ for the DAEPS results with (w/) and without (w/o) the proper boundary condition (BC): (a) mode structure for real and imaginary parts of Ψ in linear scale; (b) real part of the logarithm of mode structure; (c) real part of the logarithm of mode structure, where the black dotted line is a linear fitting of the logarithm of the mode structure with the proper BC; (d) relative error of the asymptotic behavior in logarithmic scale.

The relative error of the asymptotic behavior is shown in Fig. 4(d) for the DAEPS 375 results with and without the proper BC, denoted by the red solid line and the blue dashed 376 line, respectively. The error of the asymptotic behavior at the boundary can propagate 377 towards the ideal region, as shown in the Fig. 4(d), which could lead to a significant 378 379 error in the calculated eigenvalue when the error propagated from the inertial region is large enough to affect the mode structure in the ideal region. Since the error of the 380 asymptotic behavior decays exponentially as it propagates towards the ideal region, we 381 can set the computational domain wide enough to eliminate the inaccuracy in the ideal 382 383 region, which requires a fair amount of extra computing resources for the case without the proper BC. 384

In short, it is important to implement the correct asymptotic behavior for the following reasons: (1) the asymptotic behavior is crucial for calculating marginally unstable or damping modes when the mode structure in the inertial region is more important than that in the ideal region; (2) the computational domain needs only to cover a relatively small part of the inertial region to save computing resources; (3) the solution to the DAEPS equation can automatically satisfy the GFLDR equation when
including the correct asymptotic behavior, which can help us more easily identify the
essential EP and Alfvénic physics.

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394 V. Circulating Energetic Particle Excited TAE

The poloidal symmetry breaking of the equilibrium magnetic field, due to its non-395 uniformity in a flux surface, enables different poloidal harmonics to be coupled together, 396 which can produce not only the frequency gaps in the SAW continuous spectrum but 397 also discrete Alfvén eigenmodes which are localized in the forbidden band. The 398 toroidicity-induced Alfvén eigenmode (TAE) is the discrete mode located inside the 399 TAE gap. Since the coupling to the continuum can be ignored, the TAE is marginally 400 stable and can be easily destabilized by EPs through wave-particle resonance [1, 39]. It 401 402 is shown that TAE can cause resonant alpha particle loss even with low TAE amplitude [1, 14]. Therefore, the linear stability study of EP excited TAE is very important for the 403 steady state operation of burning plasmas. 404

The SAW continuous spectrum is important because it determines the coupling of 405 EP excited Alfvénic fluctuations to the continuous spectrum with continuum damping 406 through phase mixing and mode structure localizations [39]. As is mentioned earlier, 407 408 DAEPS can calculate marginally unstable and damping modes by incorporating the correct asymptotic behavior. As an application of this feature, we demonstrate here that 409 the DAEPS code can also calculate the Alfvén continuous spectrum by ignoring the KC 410 term and using the Floquet theory. Given toroidal and poloidal mode numbers (n,m), 411 the frequency of the Alfvén continuum at flux surface r must satisfy 412 $v^2(\omega,r) = \lceil nq(r) - m \rceil^2$. We have designed an algorithm to calculate the Floquet 413 theory v for the Alfvén continuum by linear fitting the logarithm of mode structure at 414 the sample points $\log \Psi(2n\pi + \theta_0)$, where the computational domain should be inside 415 the inertial region, $|\theta| \gg 1$. The Alfvén continuous spectrum calculated by DAEPS is 416 compared with AWC [40], which is an ideal MHD global eigenvalue code, as shown in 417

418 Fig. 5(a) with concentric circular flux surfaces, inverse aspect ratio $\epsilon = \frac{a}{R} = 0.25$,

419 toroidal mode number n = 5, and a parabolic q profile $q = 1 + \left(\frac{r}{a}\right)^2$, where *a* is the

420 minor radius. The relative error between the DAEPS and AWC result is less than 0.1%. 421 An example of the local dispersion curve of Alfvén continuous spectrum is shown in 422 Fig. 5(b). After the calculation of the local dispersion curve on the each flux surface, 423 the frequency of global Alfvén continuous spectrum of different toroidal and poloidal 424 mode numbers on the given flux surface can be calculated using the frequency at given 425 ν of the same local dispersion curve.



Figure 5: Alfvén continuous spectrum calculated by DAEPS, where the solid lines are AWC result, red circles are DAEPS result. (a) Comparison of global Alfvén continuous spectrum with AWC result. (b) Local dispersion curve of Floquet theory v at r = 0.4a or q = 1.16 surface.

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TAEs are marginally stable MHD modes, which can be easily excited by EPs, especially by circulating EPs. Therefore, the DAEPS code is first developed to calculate the TAE mode excited by the circulating energetic particles, assuming an ideal MHD background plasma and the KC term contributed by EP only. Fig. 6 shows the TAE numerical result by DAEPS with the prescribed plasma parameters s = 0.2, q = 1.2,

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$$\epsilon = 0.15$$
, $\eta_E = 0.2$, $\epsilon_{nE} \equiv \frac{L_{nE}}{R_0} = 0.2$, $k_{\theta}\rho_E = 0.4$, $v_{tE} / v_A = 0.5$ and $\alpha = 0$ which

keeps the TAE frequency above the lower Alfvén continuum. For the benchmark purpose, the equilibrium energetic particle distribution is set as Maxwellian. As shown in Fig. 6(a), the TAE growth rate almost increases with the energetic particle pressure β_E linearly, which is consistent with the previous theory [9], where the ratio between the growth rate and frequency for circulating EP excited TAE is provided by [16]:

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$$\frac{\gamma}{\omega} = \frac{4\pi^2 q^3 R}{B^2} \left\langle m_E \left(\frac{v_\perp^2}{2} + v_\parallel^2 \right)^2 Q F_{0E} \left[\delta \left(v_\parallel - v_A \right) + \frac{1}{3} \delta \left(v_\parallel - \frac{v_A}{3} \right) \right] \right\rangle_{\nu}, \quad (22)$$

444 where δ is the Dirac delta function, which shows the resonant contribution from the $v_{\parallel} = v_A / 3$ and $v_{\parallel} = v_A$ resonance, where the FLR and FOW effects are ignored in the 445 theory. To compare DAEPS results with Eq. (22) in a more rigorous way, the FLR and 446 447 FOW effects are ignored in the DAEPS equation. By substituting the frequency calculated by DAEPS into Eq. (22), we obtain the theoretical growth rate, which is then 448 compared to the growth rate from DAEPS, as shown in Fig. 6(b). The relative difference 449 in the growth rate between DAEPS and the theory is less than 1%. In addition, the 450 growth rate without FLR and FOW effects in Fig. 6(b) is 6 times larger than the growth 451 rate with FLR and FOW effects in Fig. 6(a), which suggests the stabilizing nature of 452 the FLR and FOW effects in the TAE excitation. The poloidal mode coupling caused 453 by FLR and FOW effect could have either stabilizing effect by suppressing the wave-454 particle resonance, or the destabilizing effect by involving more energetic particles in 455 the wave-particle resonance [9]. In the parameter regime of this DAEPS calculation, 456 the FLR and FOW effect is dominated by stabilization, because the stabilizing effect 457 caused by the FLR and FOW due to the $v_{\parallel} = v_A / 3$ resonance is more important than 458 the destabilizing effect due to the $v_{\parallel} = v_A / 5$ resonance as the EP distribution function 459 is set as a local Maxwellian with EP thermal velocity $v_{tE} = v_A / 2$ in this case. 460

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(a)





Figure 6: The eigen frequency of EP induced TAE varies with β_E (a) The TAE frequency and growth rate from DAEPS with FOW and FLR effects. (b) The TAE frequency and growth rate from DAEPS and theory without FOW and FLR effects.

VI. Conclusion and Discussion 469

470 In this paper, we developed a non-perturbative eigenvalue code DAEPS for the drift Alfvén energetic particle stability, and benchmarked the code with theory and other 471 numerical codes on the instabilities involving circulating particle dynamics and MHD 472 behavior, e.g., KBM, BAE and EP induced TAE, and Alfvén continuum. In the DAEPS 473 model equations, we take the ideal MHD approximation for the background plasma, 474 475 and keep the EP contribution in the kinetic compression (KC). We discussed in detail the numerical method employed in DAEPS, which uses cubic B-spline finite elements 476 477 with special treatment near the computational boundary to deal with the Dirichlet or Neumann boundary condition as required by physics. We implemented a reduced KC 478 term in the DAEPS code to accelerate the calculation of the eigen frequency, growth 479 rate and asymptotic behavior for BAE/KBM dozens of times faster than using the 480 complete KC term without losing accuracy. This makes DAEPS a practically useful 481 toolkit for the experimentalists to study Alfvén instabilities with kinetic effects. The 482 483 DAEPS result suggests that the effects of FOW and FLR can stabilize the BAE and TAE modes by suppressing the wave-particle resonance. In the DAEPS model 484 equations, the asymptotic behavior of the mode structure is properly handled. Thus the 485 486 DAEPS code can calculate marginally unstable or damping modes as well as continuous spectrum, which is absent from other codes; for unstable modes, the requirement of 487 computational domain is reduced to save computational resources substantially. 488 Furthermore, the DAEPS model equations satisfy the GFLDR equation automatically, 489 490 which is capable of locating the essential Alfvénic physics and EP behaviors. The trapped particle contribution is ignored temporarily in this paper for simplicity and will 491 be included in a future paper. In addition, the experimental equilibrium and profiles will 492 be included in the DAEPS code as well. 493

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