

# Free-boundary plasma equilibria with toroidal plasma flows

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## abstract

Magnetohydrodynamic equilibrium schemes with toroidal plasma flows and the scrape-off layer are developed for the 'divertor-type' and 'limiter-type' free boundaries in the tokamak cylindrical coordinator. With a toroidal plasma flow, the flux functions are considerably different under the isentropic and isothermal assumptions. The effects of the toroidal flow on the magnetic axis shift are investigated. In a high beta plasma, the magnetic shift due to the toroidal flow are almost the same for both the isentropic and isothermal cases, and are about  $0.04a_0$  ( $a_0$  is the minor radius) for  $M_0=0.2$  (the toroidal Alfvén Mach number on the magnetic axis). In addition, the X-point is slightly shifted upward by  $0.0125 a_0$ . But the magnetic axis and the X-point shift due to the toroidal flow may be neglected because  $M_0$  is usually less than 0.05 in a real tokamak. The effects of the toroidal flow on the plasma parameters are also investigated. The high toroidal flow shifts the plasma outward due to the centrifugal effect. Temperature profiles are noticeable different because the plasma temperature is a flux function in the isothermal case.

## I. Introduction

In the past decades, plasma flows have been observed in almost all tokamaks. It

24 can be either spontaneous[1] or driven by neutral beam injection[2] or radio frequency  
25 wave heating[3]. Some advance diagnostic technologies have been developed to  
26 measure plasma flow, such as charge exchange recombination spectroscopy (CXRS)[4],  
27 imaging x-ray crystal spectrometer (XCS)[5], Doppler coherence imaging spectroscopy  
28 (Doppler CIS)[6][7] and Langmuir probe. With diagnostic developments, the effect of  
29 plasma flows has been investigated intensively. It is found that either toroidal or  
30 poloidal plasma flows could suppress macroscopic stabilities , such as (double) tearing  
31 mode (TM)[8][9] and resistive wall mode (RWM)[10], and then largely improve both  
32 energy and momentum confinement[11][12]. The penetration properties of the  $n = 1$   
33 resonant magnetic perturbation (RMP) is also strongly correlated with toroidal  
34 flows[13][14].

35 For static and ideal plasma, the equilibrium with the axisymmetric assumption can  
36 be obtained by solving the well-known Grad-Shafranov (GS) equation that is the  
37 nonlinear elliptic partial differential equation for poloidal magnetic flux  $\psi$ . There are  
38 two free flux functions, pressure  $p(\psi)$  and poloidal current function  $F(\psi)$ , in the GS  
39 equation. Several famous static equilibrium codes, such as CHEASE[15], EFIT[16][17],  
40 HELENA[18], NOVA q-solver[19] and so on, were developed to solve the GS equation  
41 successfully. In order to consider a toroidal plasma flow in the equilibrium, the GS  
42 equation has to be generalized. Several codes, such as FLOW[20], ATEC[21],  
43 CLIO[22], FINESSE[23], and M3D equilibrium solver[24], have also been developed  
44 to solve the generalized Grad-Shafranov (GGs) equation[25][26], which is able to  
45 obtain two types of the equilibria: isentropic equilibrium and isothermal equilibrium..  
46 In the isentropic equilibrium, it is assumed that the entropy  $S=S(\psi)$  is constant on

47 magnetic surfaces, which considers the isotropic plasma and holds for isentropic flow  
48  $\mathbf{B} \cdot \nabla S(\psi) = 0$ . In the isothermal equilibrium, the plasma temperature is assumed to a  
49 surface quantity  $T=T(\psi)$  because of the large heat conductivity along the magnetic field  
50 line within a flux surface, which implies isothermal flow  $\mathbf{B} \cdot \nabla T(\psi) = 0$ . In this paper,  
51 a detailed comparison between these two equilibria is presented.

52 The boundary condition at the plasma surface can be chosen to be either a fixed  
53 boundary, where plasma-vacuum boundary is replaced by a surface of a perfect  
54 conductor[27], or a free boundary as shown in Figure 1. In this paper, we give  
55 construction schemes to solve the GGS equation for isentropic and isothermal equilibria  
56 with toroidal plasma flows for two different types of the free boundary condition. For  
57 the first type of the free boundary problem that is also called the 'limiter-type' free  
58 boundary, the plasma equilibrium is solved under an external field by imposing a  
59 constraint such as a fixed point where plasma interacts with the limiter. In the second  
60 type of the free boundary, namely the 'divertor-type' free boundary, the plasma-vacuum  
61 boundary flux value  $\psi$ , the position and the shape of plasma are unknown beforehand  
62 and defined by a set of external coils and plasma current[24][28].

63 Three-dimensional toroidal magneto-hydrodynamics code (CLT, Ci-Liu-Ti, which  
64 means magnetohydrodynamics in Chinese) has been modified to include a free-  
65 boundary equilibrium solver (called CLT-EQ) with toroidal flows and the scrape-off  
66 layer (SOL)[8]. A cylindrical coordinator ( $R, \phi, Z$ ) is used to avoid the singularity at  
67 the central point,  $r=0$ , in the toroidal coordinator ( $\psi, \theta, \xi$ ). However, the cylindrical  
68 coordinate makes the outer boundary to be more difficult handling because the plasma

69 boundary at the plasma last close surface does not locate at the grid points in the old  
70 version of CLT[8]. The current version of the CLT code has been modified with a free  
71 plasma boundary and consists of the X point, the separatrix, and the SOL. With a free  
72 plasma boundary, CLT has the capability to calculate self-consistently in the plasma  
73 edge region.

74 The rest of this paper is organized as follows: in Section II, isentropic and  
75 isothermal equilibrium formulations with a toroidal plasma flow are present. In Section  
76 III, a detail construction scheme to solve the GGS equation with a free boundary is  
77 discussed. To be more specific, different plasma regions in the computational domain  
78 are defined in order to construct the current source. The Green's function method is  
79 adopted for external coils. In Section IV, the solving procedure used in CLT-EQ is  
80 described. Numerical results of the isentropic and isothermal equilibria for the two  
81 different types of the free boundary with toroidal plasma flows are presented in Section  
82 V. The conclusion and discussion are given in Section VI.

83

## 84 **II. Formulation of Isentropic and Isothermal Equilibria for Toroidal Plasma Flow**

85 We start with the steady-state ideal magnetohydrodynamics (MHD) equations in a  
86 cylindrical coordinate  $(R, \phi, Z)$  with  $\partial/\partial\phi = 0$ . The MHD equations with plasma flows  
87 are as follows:

$$88 \quad \nabla \cdot (\rho \mathbf{v}) = 0 \quad (1)$$

$$89 \quad \rho(\mathbf{v} \cdot \nabla) \mathbf{v} = \mathbf{J} \times \mathbf{B} - \nabla p \quad (2)$$

$$90 \quad \nabla \times \mathbf{E} = 0 \quad (3)$$

91 
$$\nabla \cdot \mathbf{B} = 0 \quad (4)$$

92 
$$\mu_0 \mathbf{J} = \nabla \times \mathbf{B} \quad (5)$$

93 
$$\mathbf{E} = -\mathbf{v} \times \mathbf{B} \quad (6)$$

94 where  $\rho$ ,  $p$ ,  $\mathbf{v}$ ,  $J$ ,  $\mathbf{B}$  and  $\mathbf{E}$  are the plasma density, the pressure, the plasma flow  
95 velocity, the current density, the magnetic field, and the electric field. Let

96  $\psi(R, Z) = \int \mathbf{B} \cdot d\mathbf{s} / 2\pi = \int_0^R R' B_z dR'$  be the poloidal-disk flux[29]. Then, the magnetic

97 field can be expressed as  $\mathbf{B} = \nabla \phi \times \nabla \psi + B_\phi \mathbf{e}_\phi$ ,  $B_R = -\frac{1}{R} \frac{\partial \psi}{\partial Z}$  and  $B_Z = \frac{1}{R} \frac{\partial \psi}{\partial R}$ , where

98  $B_R$  and  $B_Z$  are the horizontal and vertical magnetic fields. From  $\mu_0 \mathbf{J} = \nabla \times \mathbf{B}$ , then

99 
$$\Delta^* \psi = -\mu_0 R J_\phi, \quad (7)$$

100 where  $J_\phi$  is the toroidal plasma current density and  $\Delta^* = R^2 \nabla \cdot (\nabla / R^2)$ . The poloidal

101 flux is able to be determined by Eq. (7), if  $J_\phi$  and the boundary condition are known. In

102 the following, we will discuss the expression of  $J_\phi$ . Faraday's law  $\nabla \times (\mathbf{B} \times \mathbf{v}) = 0$  and

103  $\mathbf{B} \cdot (\mathbf{B} \times \mathbf{v}) = 0$  imply  $\mathbf{B} \times \mathbf{v} = \Omega(\psi) \nabla \psi$ , where  $\Omega(\psi)$  is an arbitrary function of the

104 poloidal flux. If only a toroidal flow  $\mathbf{v} = v_\phi \mathbf{e}_\phi$  is considered, then

105  $\mathbf{B} \times \mathbf{v} = \nabla \phi \times \nabla \psi \times v_\phi \mathbf{e}_\phi = (v_\phi / R) \nabla \psi$ . We have

106 
$$v_\phi = R \Omega(\psi) \quad (8)$$

107 where  $\Omega(\psi)$  is the toroidal angular velocity of the flux surface[26]. Similar to the

108 poloidal flux  $\psi(R, Z)$ , we define a poloidal current function

109  $F(R, Z) = \int \mu_0 \mathbf{J} \cdot d\mathbf{s} / 2\pi = \int_0^R \mu_0 R' J_z dR'$  and then obtain  $J_z = \frac{1}{\mu_0 R} \frac{\partial F}{\partial R}$ . Using

110  $\nabla \cdot \nabla \times \mathbf{B} = \mu_0 \nabla \cdot \mathbf{J} = 0$  , we have  $J_R = -\frac{1}{\mu_0 R} \frac{\partial F}{\partial Z}$  and the poloidal current

111  $\mathbf{J}_p = (\nabla F \times \mathbf{e}_\phi) / \mu_0 R$  . From the R component of the Ampere's law Eq. (5), we get

112  $\mu_0 J_R = -(\partial F / \partial Z) / R = -\partial B_\phi / \partial Z$  , which implied

$$113 \quad F(R, Z) = RB_\phi \quad (9)$$

114 Considering  $(\mathbf{v} \cdot \nabla) \mathbf{v} = -R\Omega^2(\psi) \mathbf{e}_R$  , the  $\phi$  component of the momentum equation

115 reduces to  $(-\rho \mathbf{v} \cdot \nabla \mathbf{v} - \nabla p + \mathbf{J} \times \mathbf{B})_\phi = (\mathbf{J} \times \mathbf{B})_\phi = (\nabla \times \mathbf{B} \times \mathbf{B})_\phi = (\mathbf{B}/R) \nabla (RB_\phi) = 0$  ,

116 which means that the poloidal current function  $F(R, Z) = RB_\phi = F(\psi)$  is also an

117 arbitrary function of the poloidal flux. The momentum equation is written in the

118 following form

$$119 \quad \frac{J_\phi}{R} \nabla \psi = \nabla p - \rho R \Omega^2 \nabla R + \frac{FF'}{R^2} \nabla \psi \quad (10)$$

120 where prime ' denotes  $\partial / \partial \psi$  . From the momentum equation,

121  $\mathbf{B} \cdot \nabla p = \mathbf{B} \cdot (-\rho \mathbf{v} \cdot \nabla \mathbf{v} + \mathbf{J} \times \mathbf{B}) = \rho R \Omega^2 \mathbf{B} \cdot \nabla R \neq 0$  implies the plasma pressure is not a

122 flux surface quantity anymore.

123 The thermodynamic relationship of  $p$ ,  $\rho$  and  $T$  in the presence of the plasma

124 rotation are derived in two forms [25][26] [20] [21]. The first form is that the entropy

125  $S=S(\psi)$  is constant on magnetic surfaces, which considers isotropic plasma and holds

126 for the isentropic flow  $\mathbf{B} \cdot \nabla S(\psi) = 0$  . The other is that the plasma temperature  $T=T(\psi)$

127 is a surface quantity because of the large heat conductivity along the magnetic field line

128 within a flux surface, which implies the isothermal flow  $\mathbf{B} \cdot \nabla T(\psi) = 0$  . In this paper,

129 both of the isentropic and isothermal equilibria are developed.

130 For the isentropic case  $S(\psi)$ , the right-hand side of Eq. (10) can be written in the  
 131 following form[25][21]:

$$132 \quad \nabla p - \rho R \Omega^2 \nabla R + \frac{FF'}{R^2} \nabla \psi = \rho \nabla \theta_s(\psi) + \left( -TS' + \rho R^2 \Omega \Omega' + \frac{FF'}{R^2} \right) \nabla \psi. \quad (11)$$

133 We find that  $\theta_s(\psi) = -R^2 \Omega^2 / 2 + \frac{\gamma}{\gamma+1} S \rho^{\gamma-1}$  is a surface quantity (see Appendix).

134 Since  $\nabla \psi$  cannot be identically zero, Eq. (10) reduces to

$$135 \quad \frac{J_\phi}{R} = \rho \theta_s' - TS' + \rho R^2 \Omega \Omega' + \frac{FF'}{R^2}. \quad (12)$$

136 For the isentropic case, Eq. (7) and (12) are the general equilibrium equation of an  
 137 axisymmetric plasma with a toroidal rotation in the cylindrical coordinate, where the  
 138 entropy is assumed to be constant on magnetic surfaces. There are four arbitrary  
 139 functions  $\theta_s(\psi)$ ,  $S(\psi)$ ,  $\Omega(\psi)$  and  $F(\psi)$  in Eq. (12). If these four functions and the  
 140 boundary condition are given, the solution of Eq. (7) is solely determined.

141 (2) For the isothermal case  $T(\psi)$ , the right-hand side of Eq. (10) can be written in  
 142 the following form[25]:

$$143 \quad \nabla p - \rho R \Omega^2 \nabla R + \frac{FF'}{R^2} \nabla \psi = \rho \nabla \theta_T(\psi) + \left( \rho(1 - \ln \rho) T' + \rho R^2 \Omega \Omega' + \frac{FF'}{R^2} \right) \nabla \psi. \quad (13)$$

144 We find that  $\theta_T(\psi) = -R^2 \Omega^2 / 2 + T \ln \rho$  is also a surface quantity (see Appendix). Eq.

145 (10) is reduced to

$$146 \quad \frac{J_\phi}{R} = \rho \theta_T' + \rho(1 - \ln \rho) T' + \rho R^2 \Omega \Omega' + \frac{FF'}{R^2} \quad (14)$$

147 Similarly, for the isothermal case  $T(\psi)$ , the solution of Eq. (10) is also solely  
 148 determined if the four arbitrary functions  $\theta_T(\psi)$ ,  $T(\psi)$ ,  $\Omega(\psi)$  and  $F(\psi)$  in Eq. (14)

149 and the boundary condition are given.

150

### 151 III. The Construction Scheme for the Free Boundary Conditions

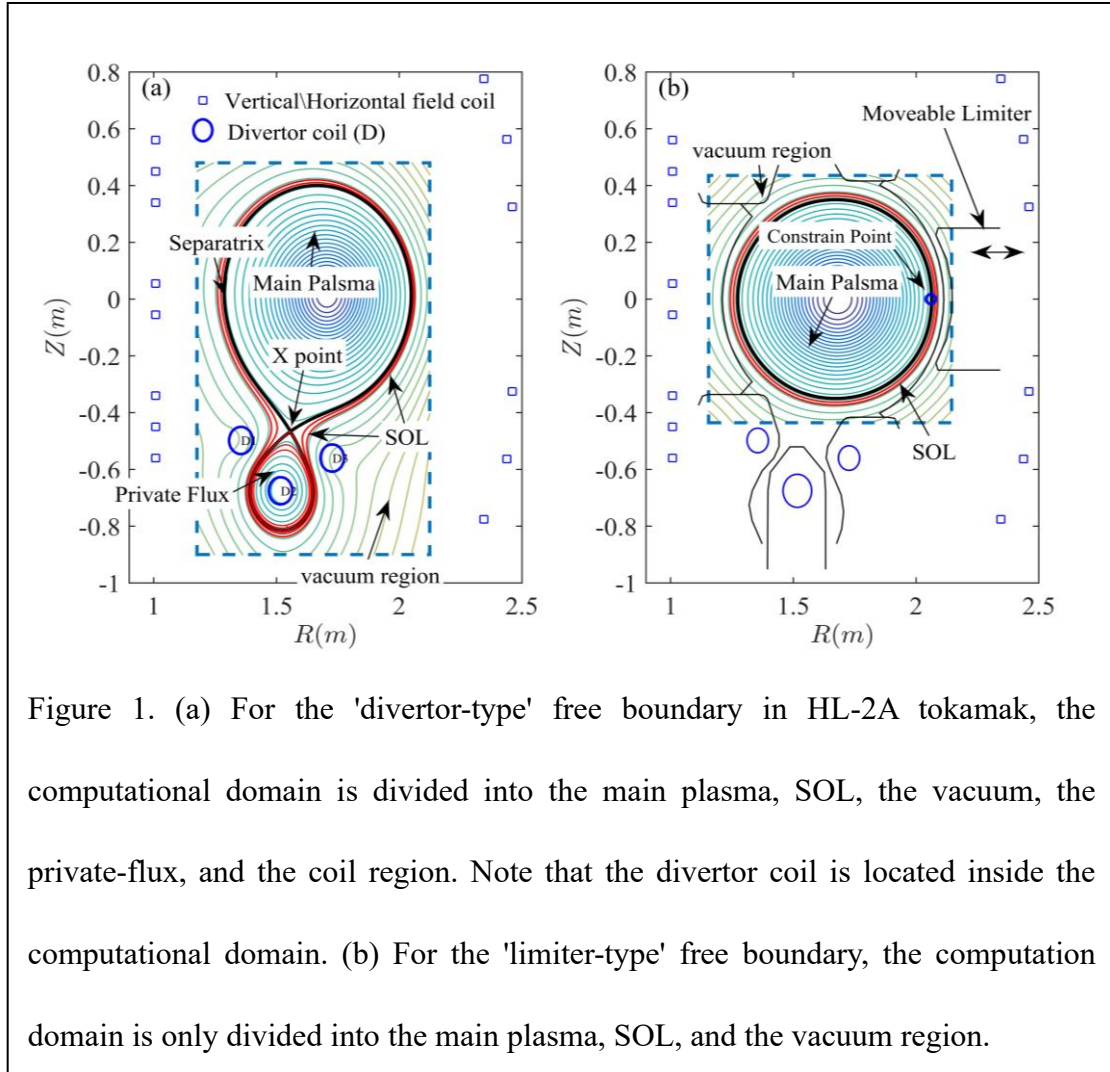


Figure 1. (a) For the 'divertor-type' free boundary in HL-2A tokamak, the computational domain is divided into the main plasma, SOL, the vacuum, the private-flux, and the coil region. Note that the divertor coil is located inside the computational domain. (b) For the 'limiter-type' free boundary, the computation domain is only divided into the main plasma, SOL, and the vacuum region.

152

153 In this section, both the 'divertor-type' and 'limiter-type' free boundary are presented. A

154 poloidal cross section of HL-2A tokamak with the divertor and the limiter are shown in

155 Figure (1). Different regions in the computational domain are defined as follow. Firstly,

156 the 'main plasma' region consists  $\tilde{\psi} < 1$ , where  $\tilde{\psi} = (\psi - \psi_{axix}) / (\psi_b - \psi_{axix})$  is the

157 normalized poloidal flux,  $\psi_{axix}$  and  $\psi_b$  are the flux at the magnetic axis and the

158 'main plasma' boundary, respectively. And  $\tilde{\psi} = 1$  represents the plasma boundary. For



159 the divertor configuration, the boundary is the separatrix or the last closed flux surface  
160 (LCFS). For the limiter, the boundary is the isoline of the constraint point where is the  
161 interface between the plasma and the limiter. Secondly, the SOL region consists of  
162  $1 < \tilde{\psi} < \tilde{\psi}_{SOL}$ .  $\tilde{\psi}_{SOL} - 1$  is the width of the SOL region that is roughly interchangeably  
163 with the power decay length  $\lambda_q$  that is designed to be about 20 mm ( $\tilde{\psi}_{SOL} \sim 1.03$ ) based  
164 on the experiment[30][31]. Thirdly, the vacuum region represents the area where the  
165 magnetic field is generated only by non-local currents, such as the plasma current and  
166 the external coil. Fourthly, the 'private flux' region (only for the divertor) consists of  
167  $\tilde{\psi} < 1$  and is located below the X point. SOL is slightly widened into the 'private flux'  
168 region. In reality, the plasma region is more complicated than the above definition when  
169 the divertor is considered[32].

170 The main plasma boundary  $\tilde{\psi}=1$  is critical for the free boundary plasma  
171 equilibrium. For the limiter-type case, the boundary is the isoline of the constraint point  
172 where is the interface between the plasma and the limiter. The plasma equilibrium is  
173 solved under the external field, as shown in Figure 1(b). It is a bit more complicated for  
174 the divertor-type case. In order to produce the real divertor configuration, we need to  
175 consider divertor coils as shown in Figure 1(a). Moreover, for the high beta plasma  
176 equilibrium, the plasma will shift toward the low field side. Therefore, vertical field  
177 coils are designed to generate the vertical magnetic field to push the plasma inward by  
178 the Lorentz magnetic force. The shape and the position of the plasma are consistent  
179 with these coil currents. According to the position of these external coil, two numerical  
180 methods are adopted. If external coils are located inside the computational domain, they  
181 are regarded as local plasma currents and the flux  $\psi$  can be computed though Eq. (16).

182 If external coils are located outside the computational domain, the Green's function  
183 method will be adopted via Eq. (19).

184

### 185 **A. Current Sources Located inside the Computational Domain**

186 Because divertor coils are located inside the computational domain for the  
187 'divertor-type' free boundary, we divide the computation domain into three parts,  
188 namely the plasma region (included the main plasma and SOL), the divertor coils region,  
189 and the vacuum region (including a part of the private flux area) as shown in Figure  
190 1(a). In the plasma region, the current source is the plasma toroidal current density  $J_\phi$   
191 in Eq. (12) or Eq. (14), so the flux function  $\psi$  satisfies Eq. (7). In the vacuum region,  
192 there is no current source, so the flux function  $\psi$  satisfies

$$193 \quad \Delta^* \psi = 0 \quad (15)$$

194 In the divertor coil region, the divertor coil currents are regarded as local plasma  
195 currents. Thus, the flux function  $\psi$  satisfies

$$196 \quad \Delta^* \psi = -\mu_0 R J_{D_i}(R, Z) \quad (i = 1, 2, 3) \quad (16)$$

197 Three divertor coils, namely D1 ( $J_{D1}$ ), D2 ( $J_{D2}$ ), and D3 ( $J_{D3}$ ), are designed in this  
198 scheme. And the coil currents  $I_{D_i} = \int J_{D_i}(R, Z) ds$ ,  $J_{D_i}$  is a parabolic distribution  
199 function. The current direction of the D1 and D3 coils must be opposite to that of the  
200 plasma current. The current direction the D2 coil is the same as that of the plasma  
201 current.

202

### 203 **B. Current Sources Located outside the Computational Domain**

204 In this case, because of vertical/horizontal field coils located outside the  
 205 computational domain as shown in Figure 1, we introduce the Green's function,

$$206 \quad G(\mathbf{x}, \mathbf{x}') = \frac{\mu_0}{2\pi} \frac{\sqrt{RR'}}{k} \left[ (2-k^2)F(k) - 2E(k) \right], \quad (17)$$

207 where  $G(\mathbf{x}, \mathbf{x}')$  is the magnetic flux at  $\mathbf{x}'=(R',Z')$  produced by the one Ampere vertical  
 208 coil current at  $\mathbf{x}=(R,Z)$ [27].  $F(k)$  and  $E(k)$  is the first and the second complete elliptic  
 209 integrals respectively, and  $k^2 = 4RR'/\left[(R-R')^2 + (Z-Z')^2\right]$ . This Green's function in  
 210 Eq. (17) satisfies

$$211 \quad \Delta^* G(\mathbf{x}, \mathbf{x}') = -\mu_0 R \delta(\mathbf{x} - \mathbf{x}') \quad (18)$$

212 Because of the current source located outside the computational domain, this  
 213 function is reduced as  $\Delta^* G(\mathbf{x}, \mathbf{x}') = 0$  in the computational domain. Therefore, the  
 214 total poloidal flux  $\psi_T$  is expressed by the Green's function in the following form

$$215 \quad \psi_T(\mathbf{x}) = \psi(\mathbf{x}) + \sum_{i=1}^N I_{coil}^i G(\mathbf{x}, \mathbf{x}'), \quad (19)$$

216 where  $I_{coil}^i$  is the  $i$ -th coils current. The Green's function method can be applied to all  
 217 poloidal field coils that are located outside the computational domain, such as  
 218 horizontal coils are used to control the plasma vertical displacement while vertical field  
 219 coils are used to control the plasma horizontal displacement.

220

#### 221 IV. Numerical Procedure

222 Figure 2 is the flowchart of the CLT-EQ code. The equilibrium equation is  
 223 computed on a  $256 \times 256$  grid of the  $(R, Z)$  plane. The solving procedure is as follows.

224 A. The four parameter functions  $\theta_s(\psi)$ ,  $S(\psi)$ ,  $\Omega(\psi)$  and  $F(\psi)$  in Eq.(12) or

225  $\theta_r(\psi)$ ,  $T(\psi)$ ,  $\Omega(\psi)$  and  $F(\psi)$  in Eq.(14) are constructed. The profile of the parameter  
226 function can be chosen to be surface-averaged data from experiment or be specially  
227 designed for simulation requirement. Moreover, the plasma flow  $\Omega$  is freely adjusted to  
228 study effects on the equilibrium by varying the plasma velocity.

229 B. The initial flux  $\psi_0$  is calculated via a set of external coils and the initial plasma  
230 current.  $\psi_0$  is critical for convergence. And it contains information of the plasma shape  
231 and displacement.

232 C. The X point, the separatrix, and the magnetic axis are calculated through the  
233 initial flux  $\psi_0$  or the updated flux  $\psi$ . In other word, the position and the flux of the X  
234 point are calculated from  $\psi_0$  or  $\psi$ , and LCFS is identified through the isoline of the X  
235 point. Then the computational domain is divided into the plasma region (including the  
236 main plasma and SOL), the vacuum region (including a part of the private flux area),  
237 and the divertor coil region. Current sources in each region are obtained via Eq. (12),  
238 or (14), (15), (16).

239 D. Eq. (7, 15, 16) are simultaneously solved using the Strongly Implicit  
240 Procedure (SIP) method to update the magnetic flux  $\psi$  [28][33][34]. In the  $n^{\text{th}}$  iteration,  
241 the iterative formula is  $\Delta^* \psi_{n+1} = -\mu_0 R J_\phi(R, \psi_n)$ . The convergence defined with a  
242 condition on the residual of this formula is  $\Delta = \sum_{i=1}^N |\psi_{n+1}^i - \psi_n^i| / N \sim 10^{-6}$ , where N is the  
243 number of grids.

244 E. Step C and D are iterated until the flux  $\psi$  at the end of Step D remains  
245 unchanged within a given tolerance.

246 F. After an equilibrium calculation, we need to check whether plasma is in a

247 reasonable position. If not, external coil currents need to be adjusted in order to obtain  
248 a suitable plasma position shown in Figure (3). Meanwhile, the initial poloidal flux  $\psi_0$   
249 is recalculated at Step B. Consequently, the new flux  $\psi$  is updated by iteration of Step  
250 C, D and E again. In the free-boundary calculation, the boundary condition is imposed  
251 during initialization. The X point, the magnetic axis, and the separatrix are not fixed  
252 and determined as a part of the solution of the equilibrium problem. Figure 3 is a high  
253 beta H-mode equilibrium. In this case, vertical field coil currents produce the vertical  
254 magnetic to put the plasma inward by the Lorentz force. Otherwise, the plasma will  
255 move to the low field side due to a large thermodynamic force. We note that the  
256 boundary is a constraint by a fixed point for the limiter-type case, while the X point is  
257 free for the divertor-type case.

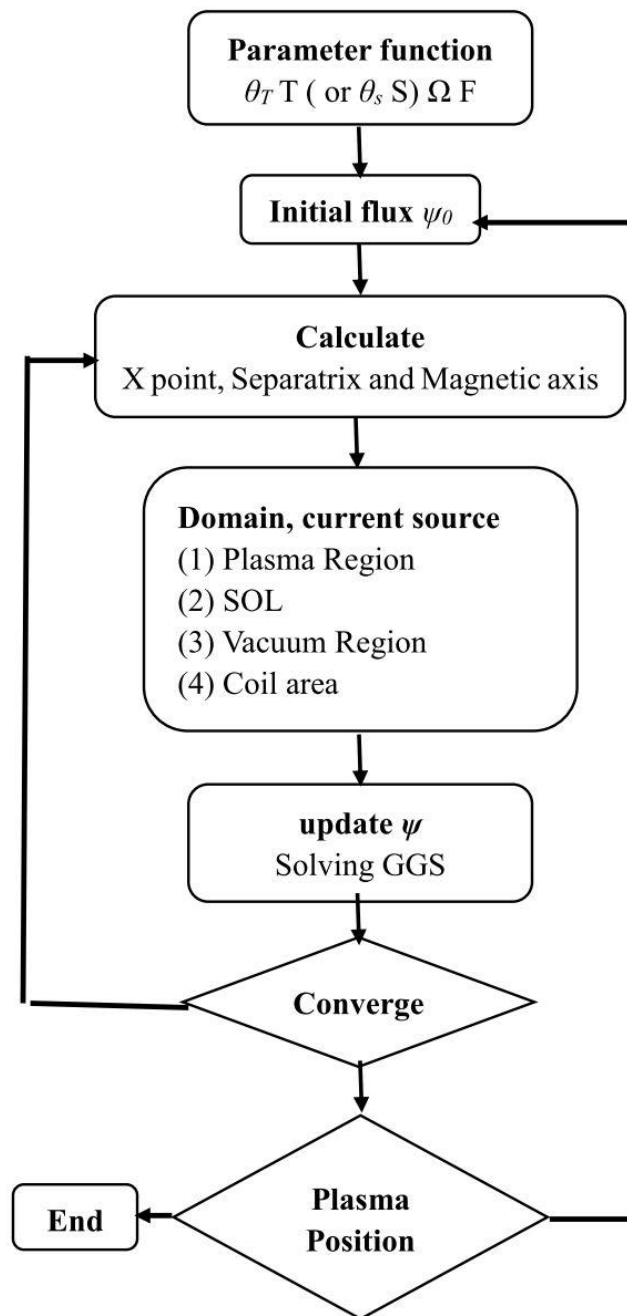


Figure 2. Flowchart of CLT-EQ

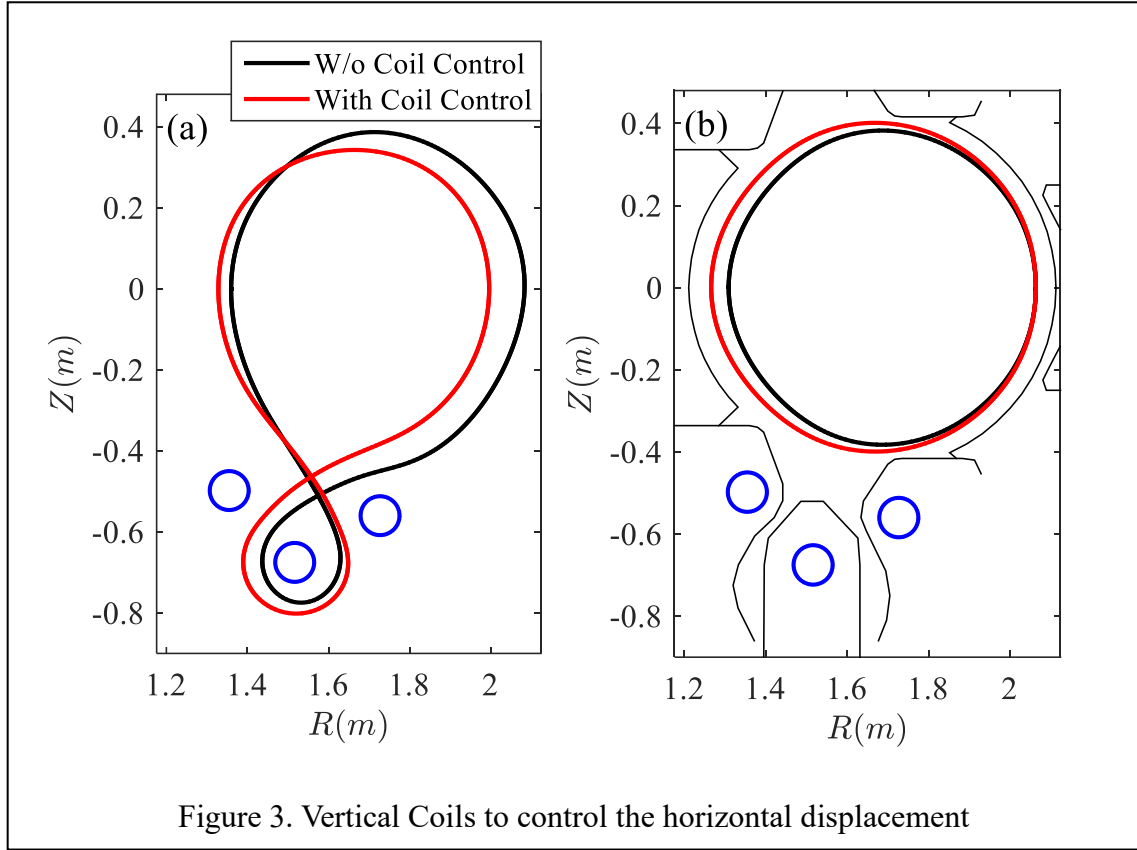


Figure 3. Vertical Coils to control the horizontal displacement

259

260

## 261 V. Numerical Results

### 262 A. Effect of Toroidal Plasma Flow on Magnetic Shift

263 As we known, the magnetic axis is displaced due to the plasma pressure and the

264 internal inductance, which is named as the Shafranov shift. With the toroidal plasma

265 rotation, the moment equation Eq. (2) can roughly be expressed as

266  $\sim \mathbf{J} \times \mathbf{B} - \nabla [p + \rho(v^2/2)]$ , which means that the 'kinetic energy' density,  $\rho(v^2/2)$ , like

267 the plasma pressure, also contributes to the Shafranov shift. In order to investigate the

268 effect of the toroidal flow on the magnetic axis shift, we use the toroidal Alfvén Mach

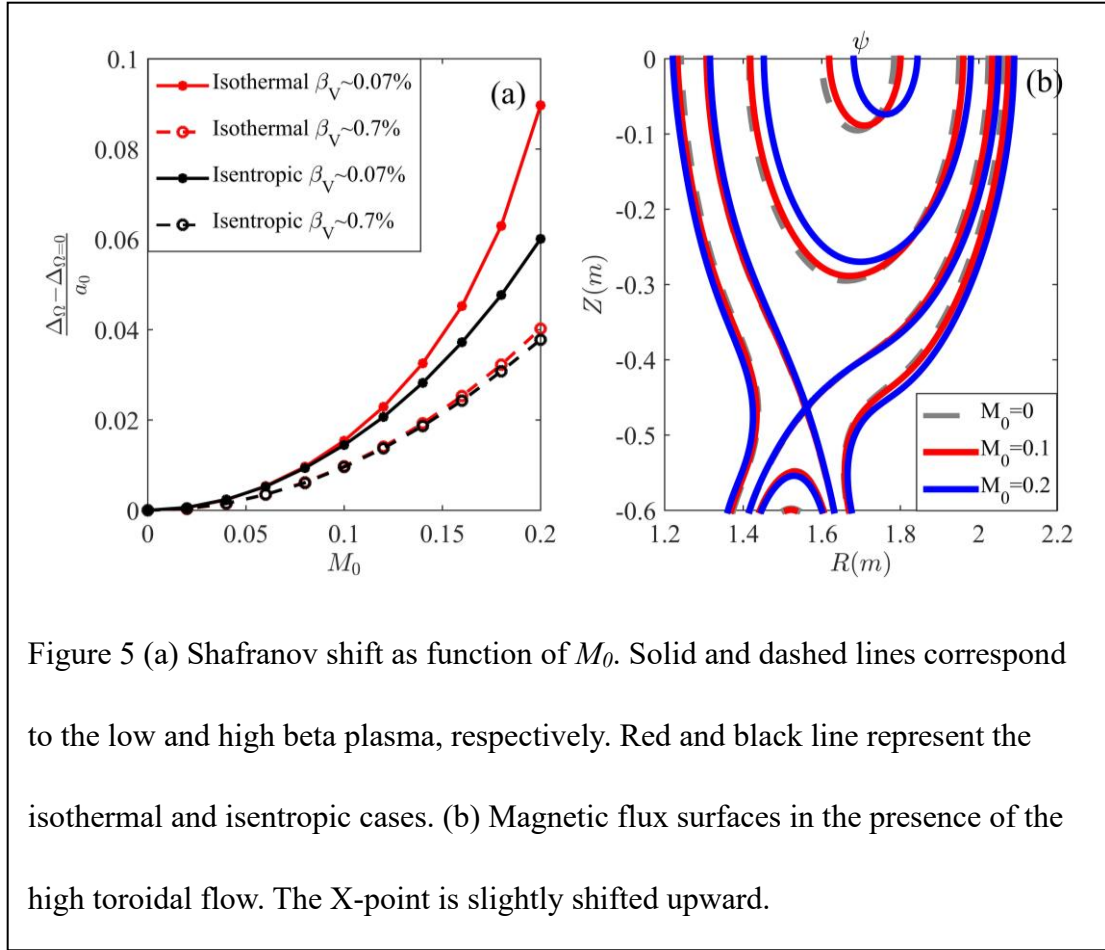
269 number,  $M = v_\phi/v_A$ , to quantify the plasma flow.  $v_A$  is the Alfvén speed and  $M_0$  is the

270 toroidal Alfvén Mach number on the magnetic axis. In order to concentrate on the

271 contribution of the toroidal flow in the Shafranov shift, we subtract the Shafranov shift

272 in the static equilibria  $\Delta_{\Omega=0}$  from the total shift  $\Delta_{\Omega}$ , and normalize with the plasma  
273 minor radius  $a_0$ . The expression  $(\Delta_{\Omega} - \Delta_{\Omega=0})/a_0$  quantifies the contribution of the  
274 toroidal plasma flow to the Shafranov shift as shown in Fig. 4(a) where the red and  
275 black lines represent for the isothermal and isentropic cases, respectively. The solid and  
276 dashed lines correspond to low beta and high beta plasma, respectively. The magnetic  
277 shift is larger at a lower beta plasma or a higher  $M_0$  for both isothermal and isentropic  
278 cases, which is not surprising since the "kinetic energy" term, compared with the  
279 pressure term in moment equation, will become more important with the plasma beta  
280 decrease or the toroidal flow (or  $M_0$ ) increase. In addition, in the low beta plasma, the  
281 magnetic shift in the isothermal case is larger than that in the isentropic case. This  
282 difference is more severe when  $M_0$  increases. However, it is seen that the effect of the  
283 toroidal rotation on the shift in the high beta plasma is qualitatively similar for both  
284 cases. The magnetic shift due to the toroidal flow is about  $0.04a_0$  at  $M_0=0.2$ . Of more  
285 interest is the shift of the X-point due to the toroidal plasma flow as shown in Figure  
286 4(b), which is only calculated in the 'divertor-type' free boundary equilibrium. The X-  
287 point is slightly shifted upward by about  $0.0125 a_0$  for both the isentropic and  
288 isothermal cases at  $M_0=0.2$ . In reality,  $M_0$  is almost less than 0.05 for most of present  
289 tokamaks[11]. Therefore, the effect of the toroidal flow on the magnetic axis and the X-  
290 point shift may be neglected.



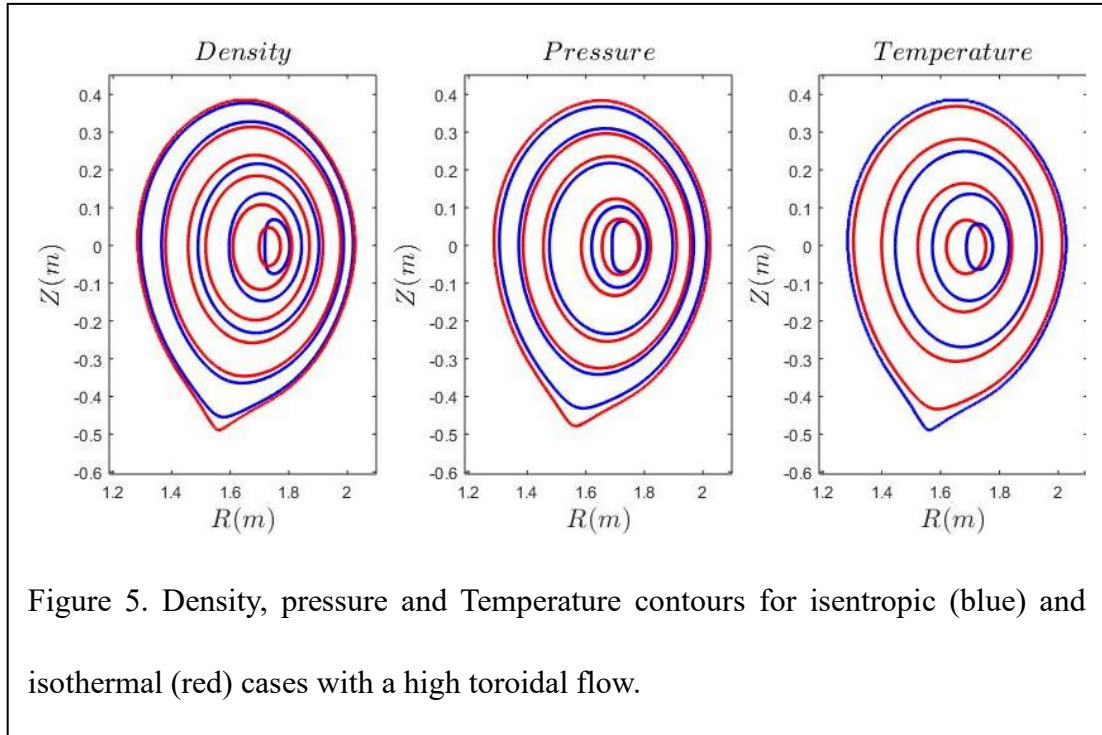


291

292

### 293 B. Effect of Toroidal Flow on Plasma Parameters

294 The effects of the toroidal flow on Plasma parameters, such as the density, the  
 295 pressure, and the temperature, are shown in Figure 5 where the red and blue lines  
 296 represent for the isothermal and isentropic cases, respectively. As we can see that  
 297 toroidal flow shifts the plasma outward due to the centrifugal effect that is qualitatively  
 298 similar both in the isothermal and isentropic cases. But there is a noticeable difference  
 299 in the temperature profile due to the fact that the plasma temperature is a flux function  
 300 regardless of the flow in the isothermal case. Because the temperature expresses as  
 301  $T = \rho^{\gamma-1}/(\gamma-1)$  in the isotropic case, the profile shift in the temperature is similar to  
 302 that in the plasma density.



303

304

## 305 VI. Conclusion and Discussion

306 In the paper, an extension of the CLT code to include a free-boundary equilibrium

307 solver with a toroidal plasma flow and SOL, called CLT-EQ, was present. There are

308 two kinds of construction schemes for the free boundary, namely 'divertor-type' and

309 'limiter-type'. Different regions, included the main plasma, SOL, the vacuum, and the

310 'private flux' region, are defined in the computational domain in order to design current

311 sources. The Green's function method is adopted for external coils if these coils are

312 located outside the computational domain. With toroidal plasma flow, the flux function

313 is considerably different under the isentropic and isothermal assumptions. For the

314 isentropic case, the entropy  $S(\psi)$  is constant on magnetic surfaces. Four arbitrary

315 functions  $\theta_s(\psi)$ ,  $S(\psi)$ ,  $\Omega(\psi)$  and  $F(\psi)$  are pre-required for an equilibrium. For the

316 isothermal case, the plasma temperature  $T(\psi)$  is a surface quantity due to large heat

317 conductivity along magnetic field lines. Another four arbitrary functions  $\theta_r(\psi)$ ,  $T(\psi)$ ,  
318  $\Omega(\psi)$  and  $F(\psi)$  are needed. The effects of the toroidal plasma flow on the Shafranov  
319 shift are investigated. In a high beta plasma, the magnetic shift due to the toroidal  
320 plasma flow are almost same for both the isentropic and isothermal cases and are about  
321  $0.04a_0$  at  $M_0=0.2$ . In addition, the X-point are slightly shifted upward by  $0.0125 a_0$ . But  
322 in fact, the effect of the toroidal flow on the magnetic axis and the X-point shift may be  
323 neglected because  $M_0$  is usually less than 0.05 in real tokamaks. The effects of the  
324 toroidal plasma flow on plasma parameters, such as the density, the pressure, and the  
325 temperature, are also investigated. The high toroidal flow shifts the plasma outward due  
326 to the centrifugal effect. But temperature profiles are noticeable difference in two cases  
327 because the plasma temperature is the flux function in the isothermal case.

328

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333

### 334 **Appendix**

335 From the well-known thermodynamic relations

$$336 \quad dh = dp/\rho + TdS$$

337 where  $h$  is the specific enthalpy. Considering the isentropic problem  $dS=0$  and then

338  $p = S\rho^\gamma$ ,  $T = \rho^{\gamma-1}/(\gamma-1)$  [25][21], the following relation can be obtained:

339

$$h = \frac{\gamma}{\gamma-1} S \rho^{\gamma-1}$$

340

where  $\gamma$  is the ratio of specific heat that is chosen to be 5/3 as usual. Considering

341

the isentropic equilibrium with  $\mathbf{v} \cdot \nabla S(\psi) = 0$ , and multiplying the momentum

342

equation by  $\rho^{-1} \mathbf{B}$ , the following expression is obtained by using

343

$\mathbf{v} \cdot \nabla \mathbf{v} = -R\Omega^2(\psi) \nabla R$  and  $\mathbf{B} \cdot \nabla \Omega = 0$

344

$$\begin{aligned} 0 &= \rho^{-1} \mathbf{B} \cdot (\rho \mathbf{v} \cdot \nabla \mathbf{v} + \nabla p - \mathbf{J} \times \mathbf{B}) \\ &= \mathbf{B} \cdot \left( \frac{\nabla p}{\rho} - \nabla R^2 \Omega^2 / 2 \right) \\ &= \mathbf{B} \cdot \nabla \left( h - R^2 \Omega^2 / 2 \right), \end{aligned}$$

345

which suggests that the Bernoulli equation is an arbitrary function of the poloidal flux,

346

i.e.,

347

$$\theta_s(\psi) = h - R^2 \Omega^2 / 2 = \frac{\gamma}{\gamma+1} S \rho^{\gamma-1} - R^2 \Omega^2 / 2$$

348

Now let us consider the isothermal equilibrium  $T(\psi)$ . The plasma is assumed an

349

ideal gas,  $p(R, \psi) = T(\psi) \rho(R, \psi)$ . Multiplying the momentum equation by  $\rho^{-1} \mathbf{B}$ ,

350

the following expression is obtained by using  $\mathbf{v} \cdot \nabla \mathbf{v} = -R\Omega^2(\psi) \nabla R$  and  $\mathbf{B} \cdot \nabla T = 0$

351

$$\begin{aligned} 0 &= \rho^{-1} \mathbf{B} \cdot (\rho \mathbf{v} \cdot \nabla \mathbf{v} + \nabla p - \mathbf{J} \times \mathbf{B}) \\ &= \mathbf{B} \cdot (-R\Omega^2 \nabla R + \nabla \rho T / \rho) \\ &= \mathbf{B} \cdot (-\nabla R^2 \Omega^2 / 2 + T \nabla \rho / \rho) + R^2 \Omega \mathbf{B} \cdot \nabla \Omega + \mathbf{B} \cdot \nabla T \\ &= \mathbf{B} \cdot (-\nabla R^2 \Omega^2 / 2 + T \nabla \ln \rho + \ln \rho \nabla T) \\ &= \mathbf{B} \cdot \nabla (T \ln \rho - R^2 \Omega^2 / 2), \end{aligned}$$

352

which indicates that  $\theta_t(\psi) = T \ln \rho - R^2 \Omega^2 / 2$  is also an arbitrary function of the

353

poloidal flux. In order to ensure the flux surface quantity of  $\theta_t(\psi)$ , we need to

354 carefully construct a density distribution function  $\rho(R, \psi)$ . With a referenced density  
 355 distribution  $\rho_0(\psi)$ , we have

$$356 \quad \theta_{T_0}(\psi) = T \ln \rho_0(\psi) - \Omega^2 R_0^2 / 2$$

357  $R_0$  is the major radius. Thus, the density that is not a flux surface quantity can be  
 358 expressed as follows,

$$359 \quad \rho(\psi, R) = \rho_0(\psi) \exp\left(\frac{\Omega^2 (R^2 - R_0^2)}{2T}\right)$$

360 And similarly, the pressure can also be expressed to be

$$361 \quad p(\psi, R) = p_0(\psi) \exp\left(\frac{\Omega^2 (R^2 - R_0^2)}{2T}\right)$$

362 Note that the relation  $p_0(\psi) = T(\psi) \rho_0(\psi)$  must be satisfied. In other words,  
 363 only two of the three parameters  $p_0(\psi)$ ,  $\rho_0(\psi)$  and  $T(\psi)$  can be chosen freely.

364  $\theta_T(\psi)$  constructed by this method can easily be proved to be the flux surface quantity,

$$\begin{aligned} & \theta_T(\psi) = T \ln \rho(R, \psi) - R^2 \Omega^2 / 2 \\ 365 \quad & = T \ln \left( \rho_0(\psi) \exp\left(\frac{\Omega^2 (R^2 - R_0^2)}{2T}\right) \right) - R^2 \Omega^2 / 2 \\ & = T \ln \rho_0 - \Omega^2 R_0^2 / 2 \\ & = \theta_{T_0}(\psi). \end{aligned}$$

366

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